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PROPAGATION OF MULTIWAVELENGTH LASER  
RADIATION THROUGH ATMOSPHERIC TURBULENCE

J. Richard Kerr, et al

Oregon Graduate Center

Prepared for:

Rome Air Development Center  
Defense Advanced Research Projects Agency

July 1975

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Technical Report  
July 1975



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THROUGH ATMOSPHERIC TURBULENCE

Oregon Graduate Center

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Project Engineer

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| 1. REPORT NUMBER<br>RADC-TR-75-181   | 2. GOVT ACCESSION NO. | 3. RECIPIENT'S CATALOG NUMBER  |
| 4. TITLE (and Subtitle)<br>PROPAGATION OF MULTIWAVELENGTH LASER RADIATION<br>THROUGH ATMOSPHERIC TURBULENCE  |                       | 5. TYPE OF REPORT & PERIOD COVERED<br>Interim Technical Report<br>1 Sep 74 - 31 Mar 75 |
|  |                       | 6. PERFORMING ORG. REPORT NUMBER<br>N/A  |
| 7. AUTHOR(s)<br>J. Richard Kerr                      Richard A. Elliott<br>James R. Dunphy                      Philip A. Pincus   |                       | 8. CONTRACT OR GRANT NUMBER(s)<br>F30602-74-C-0082                                     |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS<br>Oregon Graduate Center<br>19600 N. W. Walker Road<br>Beaverton OR 97005   |                       | 10. PROGRAM ELEMENT, PROJECT, TASK<br>AREA & WORK UNIT NUMBERS<br>62301E<br>12790212   |
| 11. CONTROLLING OFFICE NAME AND ADDRESS<br>Defense Advanced Research Projects Agency<br>1400 Wilson Boulevard<br>Arlington VA 22209  |                       | 12. REPORT DATE<br>July 1975   |
|  |                       | 13. NUMBER OF PAGES<br>49  |
| 14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)<br>Rome Air Development Center (OCSE)<br>Griffiss AFB NY 13441   |                       | 15. SECURITY CLASS. (of this report)<br>UNCLASSIFIED                                   |
|  |                       | 15a. DECLASSIFICATION DOWNGRADING<br>SCHEDULE<br>N/A                                   |
| 16. DISTRIBUTION STATEMENT (of this Report)<br><br>Approved for public release; distribution unlimited.  |                       |  |
| 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)<br>Same   |                       |  |
| 18. SUPPLEMENTARY NOTES<br>RADC Project Engineer:<br>Capt. Darryl P. Greenwood (OCSE)  |                       |  |
| 19. KEY WORDS (Continue on reverse side if necessary and identify by block number)<br>Propagation<br>Turbulence<br>Atmospheric Optics<br>Scintillation   |                       |  |
| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)<br>Recent work on the short-term statistics of scintillation is extended to a more detailed investigation of the effective number of independent turbulence regions on a propagation path as a function of wind direction and other parameters. The resultant effect on the spread in strength-of-fluctuation measurements vs. averaging time is discussed, including both microthermal and scintillation data and their interrelationship. These considerations are related to spatial correlation measurements of the turbulence strength (microthermal envelope) as |                       |  |

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a function of averaging time, including the influence of pronounced intermittency of turbulence.

In a related discussion, the conditional statistics of scintillation, based on an initial comparison of the instantaneous target irradiance with a pre-determined threshold level, are investigated as a function of elapsed time. With the assumption that the two-point log scintillation process is a bivariate normal, the problem is readily solvable using empirically derived correlation functions. The validity and limitations of this assumption are briefly considered, and representative results are given.

New multiwavelength facilities are described which will be used for the completion of the experiments on mean target irradiance and its fluctuations, with and without cancellation of turbulence-induced beam wander. Other near-term plans are also briefly reviewed.

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PROPAGATION OF MULTIWAVELENGTH LASER RADIATION  
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Contractor: Oregon Graduate Center  
Contract Number: F30602-74-C-0082  
Effective Date of Contract: 1 December 1973  
Contract Expiration Date: 31 July 1975  
Amount of Contract: \$129,699.00  
Program Code Number: 4E20  
Period of work covered: 1 Sep 74 - 31 Mar 75

Principal Investigator: Dr. J. Richard Kerr  
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This research was supported by the Defense  
Advanced Research Projects Agency of the  
Department of Defense and was monitored by  
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### Summary

Recent work on the short-term statistics of scintillation is extended to a more detailed investigation of the effective number of independent turbulence regions on a propagation path as a function of wind direction and other parameters. The resultant effect on the spread in strength-of-fluctuation measurements vs. averaging time is discussed, including both microthermal and scintillation data and their inter-relationship. These considerations are related to spatial correlation measurements of the turbulence strength (microthermal envelope) as a function of averaging time, including the influence of pronounced intermittency of turbulence.

In a related discussion, the conditional statistics of scintillation, based on an initial comparison of the instantaneous target irradiance with a predetermined threshold level, are investigated as a function of elapsed time. With the assumption that the two-point log scintillation process is a bivariate normal, the problem is readily solvable using empirically derived correlation functions. The validity and limitations of this assumption are briefly considered, and representative results are given.

New multiwavelength facilities are described which will be used for the completion of the experiments on mean target irradiance and its fluctuations, with and without cancellation of turbulence-induced beam wander. Other near-term plans are also briefly reviewed.



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## I. INTRODUCTION

This report will briefly summarize recent progress and ongoing efforts on several topics in optical propagation through atmospheric turbulence. In Section II, we describe some further results on the short-term statistics of turbulence and scintillation, which supplements the detailed treatment given in the preceding report on this program. In Section III, we discuss a new topic, the conditional fading statistics of a scintillating signal or target illumination, in which the state of the "channel" is investigated immediately following the onset of a "good" interval. Finally, in Section IV we describe new experimental work and facilities, including multiwavelength target-irradiance investigations with beam-wander cancellation, very-long-path or strong-scattering scintillation phenomena, and other areas of interest.

## II. FURTHER RESULTS ON SHORT-TERM STATISTICS

In the preceding technical report on this program,<sup>1</sup> we presented a complete theoretical treatment of the short-term statistics of turbulence and scintillation, including data-spread and confidence-interval considerations as a function of averaging time. In this section, we supplement the previous discussion with representative results of recent experiments on this topic. Our related work on computer simulation of the short-term propagation problem will be described in a subsequent report.

### A. Relationship Between Microthermal and Scintillation Data Spread

In a discretized model of the propagation path,<sup>1</sup> we idealize the turbulence into  $N$  elements, the strength of turbulence being totally correlated throughout one element and totally uncorrelated between any two elements. The length of an element depends on the averaging time

-----

1. J. R. Kerr, et al, "Propagation of Multiwavelength Laser Radiation Through Atmospheric Turbulence," RADC-TR-74-320, November, 1974.



( $\tau$ ) used in determining "strength of turbulence" ( $C_{n\tau}^2$ ), and on the direction of the wind relative to the path. The variance of a set of measurements of the scintillation log amplitude variance ( $\text{Var } \sigma_\tau^2$ ) is then related to the variance of microthermal measurements ( $\text{Var } C_{n\tau}^2$ ) by

$$\frac{\text{Var } \sigma_\tau^2}{\sigma^2} = \frac{\text{Var } C_{n\tau}^2}{C_n^2} \cdot \frac{1}{N_{\text{eff}}} \quad (1)$$

The quantity  $N_{\text{effective}}$  is derived from  $N$ , the number of correlation lengths of  $C_{n\tau}^2$  along the path, and the spatial weighting function ( $f$ ) determined by beam geometry. If the log amplitude variance is written as

$$\sigma^2 = \sum_{i=1}^N f_i C_{n_i}^2 \quad (2)$$

then we have

$$N_{\text{eff}} = \frac{\left( \sum_{i=1}^N f_i \right)^2}{\sum_{i=1}^N f_i^2} \leq N \quad (3)$$

For a spherical wave,  $f$  is a discrete approximation to

$$f(z) \sim \left( \frac{z}{L} \right)^{5/6} (L-z)^{5/6} \quad (4)$$



where  $z$  is the path variable and  $L$  is the total pathlength. In the case of e.g. focused beams or other systems yielding more localized weighting functions,  $N_{\text{eff}}$  becomes much less than  $N$  and  $\text{Var } \sigma_{\tau}^2$  increases accordingly. In the limit of  $f$  as a delta function, the variance in  $\sigma_{\tau}^2$  for any given  $\tau$  will be the same as that for  $C_{n\tau}^2$ .

For averaging times greater than the integral scale of the squared microthermal fluctuations ( $I_{\Delta T}^2$ ), the normalized variance of  $C_{n\tau}^2$  measurements will be inversely proportional to  $\tau$  (Ref. 1). The corresponding dependence for the normalized variance of  $\sigma_{\tau}^2$  depends on the wind field. If we extend our idealization to assume large-scale regular flow with "frozen-in" strength of turbulence over scales comparable with the pathlength, we may distinguish the following two cases:

1. When the wind is parallel to the path, the  $z$ -correlation length of  $C_{n\tau}^2$  is proportional to  $\tau$ , which cancels the usual effect of increased averaging, and thus  $\text{Var } \sigma_{\tau}^2$  is independent of  $\tau$ . That is,  $N \sim \tau^{-1}$ , to be consistent with Eq. 1.
2. When the wind is perpendicular to the path, the  $z$ -correlation length is independent of  $\tau$ ,  $\text{Var } \sigma_{\tau}^2 \sim \tau^{-1}$ , and  $N$  is independent of  $\tau$ .

When we compare this useful but idealized conceptual model to experimental data, subtleties and complications immediately arise, as shown by the following examples. In Table I, we show the basic parameters of nine experimental runs comparing normalized  $C_{n\tau}^2$  and  $\sigma^2$  variances vs. averaging time. Runs 1-6 involve winds basically parallel to the path, and the results for  $1/N_{\text{eff}}$  (Eq. 1) are shown in Fig. 1a. According to the foregoing reasoning, we would ideally expect a slope of +1 for these curves, and a tendency to break in this direction may be noted. In Fig. 1b, curves are given for wind directions partially or entirely perpendicular to the path; two of these tend to be flat, as expected. Taking into account all conditions and averaging times, values of  $N_{\text{eff}}$  were seen to range from approximately 8 to 200.



TABLE I

Parameters for Data on Var  $C_{n_T}^2$  and Var  $\sigma_T^2$  Shown in Figs. 1, 2.

| <u>Run No.</u> | <u>Symbol on Figs.</u> | <u>v(m/sec)</u> | <u>Wind Direction<br/>Relative to<br/>Optical Path</u> | <u><math>\overline{\sigma^2}</math></u> |
|----------------|------------------------|-----------------|--|---|
| 1              | ○                      | 3.5             | 0°   | 0.31                                    |
| 2              | □                      | <1              | 0°   | 0.24                                    |
| 3              | ◇                      | 3               | 0°   | 0.28                                    |
| 4              | △                      | 3.5             | 180°   | 0.30                                    |
| 5              | +                      | 9               | -15°   | 0.076                                   |
| 6              | *                      | 3.5             | 195°   | 0.31                                    |
| 7              | ●                      | 4               | -45°   | 0.25                                    |
| 8              | ▲                      | 0.5-2           | 90°  | 0.33                                    |
| 9              | ■                      | 1.5             | 90°  | 0.32                                    |

Wavelength: 4880Å

Pathlength: 1.6 km

Beam Geometry: Approximate Spherical Wave



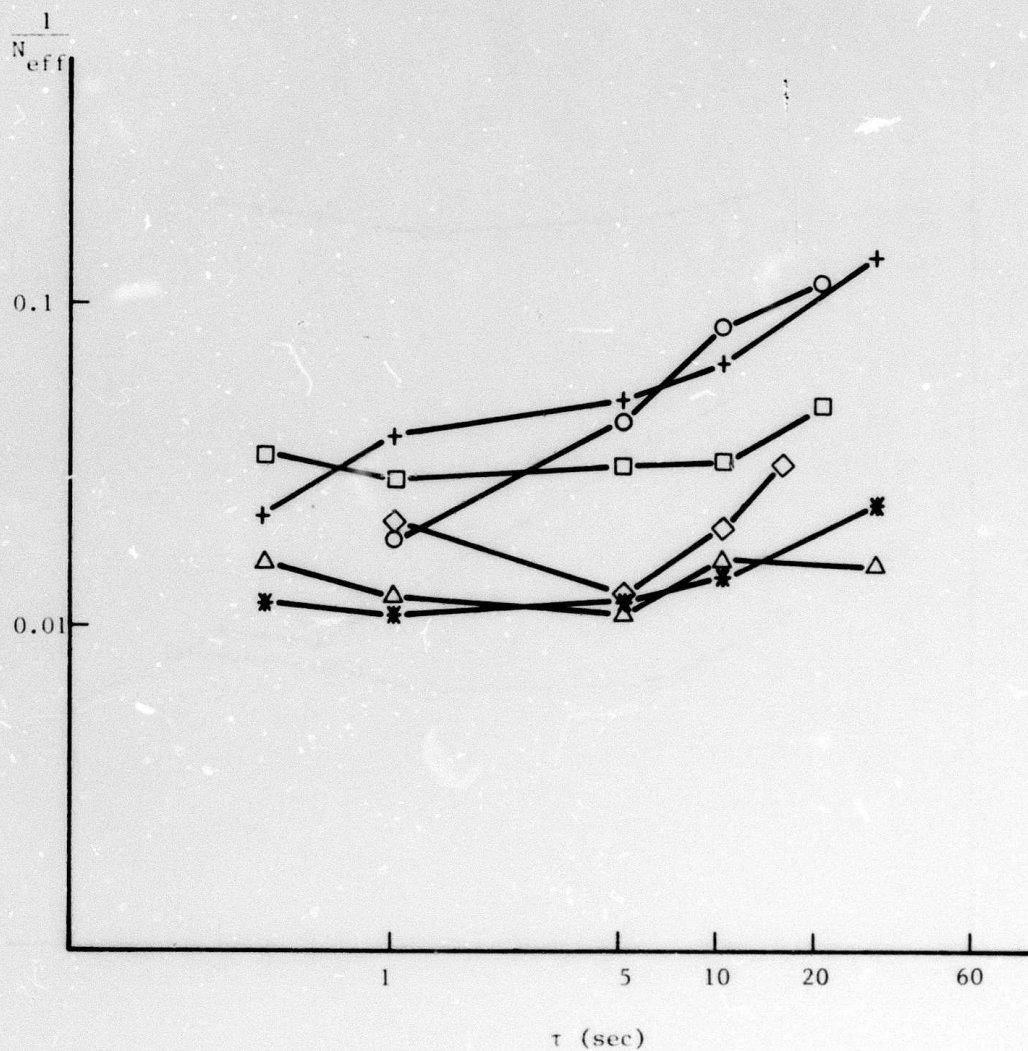


Figure 1a. The reciprocal number of effectively-independent turbulence regions  $\left( \frac{1}{N_{\text{eff}}} \right)$  along a propagation path, vs. averaging time

$(\tau)$ . The runs are identified by the symbols in Table I. Wind parallel to path.



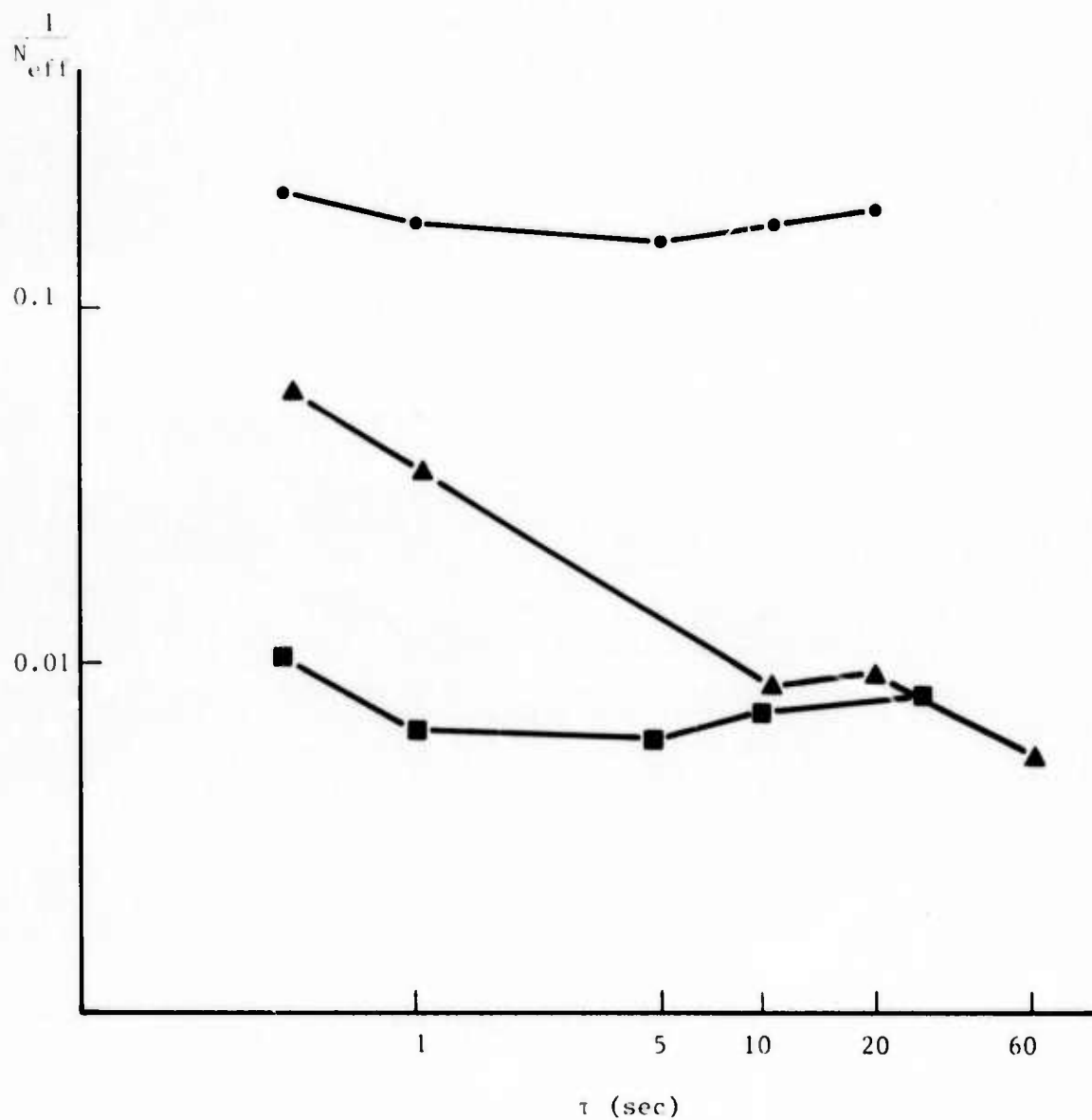


Figure 1b. The reciprocal number of effectively-independent turbulence regions  $\left(\frac{1}{N_{eff}}\right)$  along a propagation path, vs. averaging time ( $\tau$ ). The runs are identified by the symbols in Table I. Wind components normal to the path.



We now examine the results for  $\text{Var } C_n^2$  alone (Fig. 2a). The slopes are in general less than the expected  $\tau$  value of (minus) one, suggesting that  $\tau$  is not in general  $\gg I_{\Delta T^2}$ . If the wind speed is  $v$ , the value of  $v I_{\Delta T^2}$  is a function of the degree of spatial intermittency of the turbulence (Ref. 1), and in some of the curves may be indicated by a breakpoint in Fig. 2a.

The results for  $\text{Var } \sigma_\tau^2$  likewise do not show the simple behavior of the idealized model (Fig. 2b). We point out three complicating factors:

1. A real wind field may be expected to be irregular over the scales of interest here, so that regions of given turbulence strength are not "frozen-in". This will cause a tendency for a (-1) rather than (0) slope for parallel wind in Fig. 2b.
2. If  $\tau$  is not  $\gg I_{\Delta T^2}$ , or if there are large-scale correlations for low spatial frequencies in  $\Delta T^2$ , the slopes in Fig. 2b will tend towards zero. This will be especially noticeable for transverse wind, where they would otherwise be (-1), and this is evident for runs 7 and 9.
3. For small  $\tau$  ( $\ll I_{\Delta T^2}$ ) on the scale of the actual scintillations themselves, Eq. 14a of Ref. 1 will apply, and slopes will tend to (-1) as in Fig. 2b. However, these shorter averaging times are not generally useful for indications of  $C_n^2$  or  $\sigma^2$ .

#### B. Microthermal Envelope Correlations

These subtleties can be further explored using spaced microthermal-probe-pair measurements of  $C_n^2$  correlations vs. averaging time. The measurement scheme is described in Fig. 13 of Ref. 1. In Figs. 3a, b correlations of the mean-square fluctuations  $\overline{\Delta T^2}|_\tau$  ( $\sim C_n^2$ ) are given for three values of  $\tau$ , for separations nearly parallel to the wind direction (the line along which the respective probe pairs are situated is slightly offset from the wind vector to preclude wake effects from the instruments). The basic spatial integral scale of  $\Delta T^2$  can be deduced from the lowest or  $\tau = 0.4$  sec curve, and the tendency of the integral scale to become equal to  $v \tau/2$  for larger  $\tau$  is evident from the other two curves.



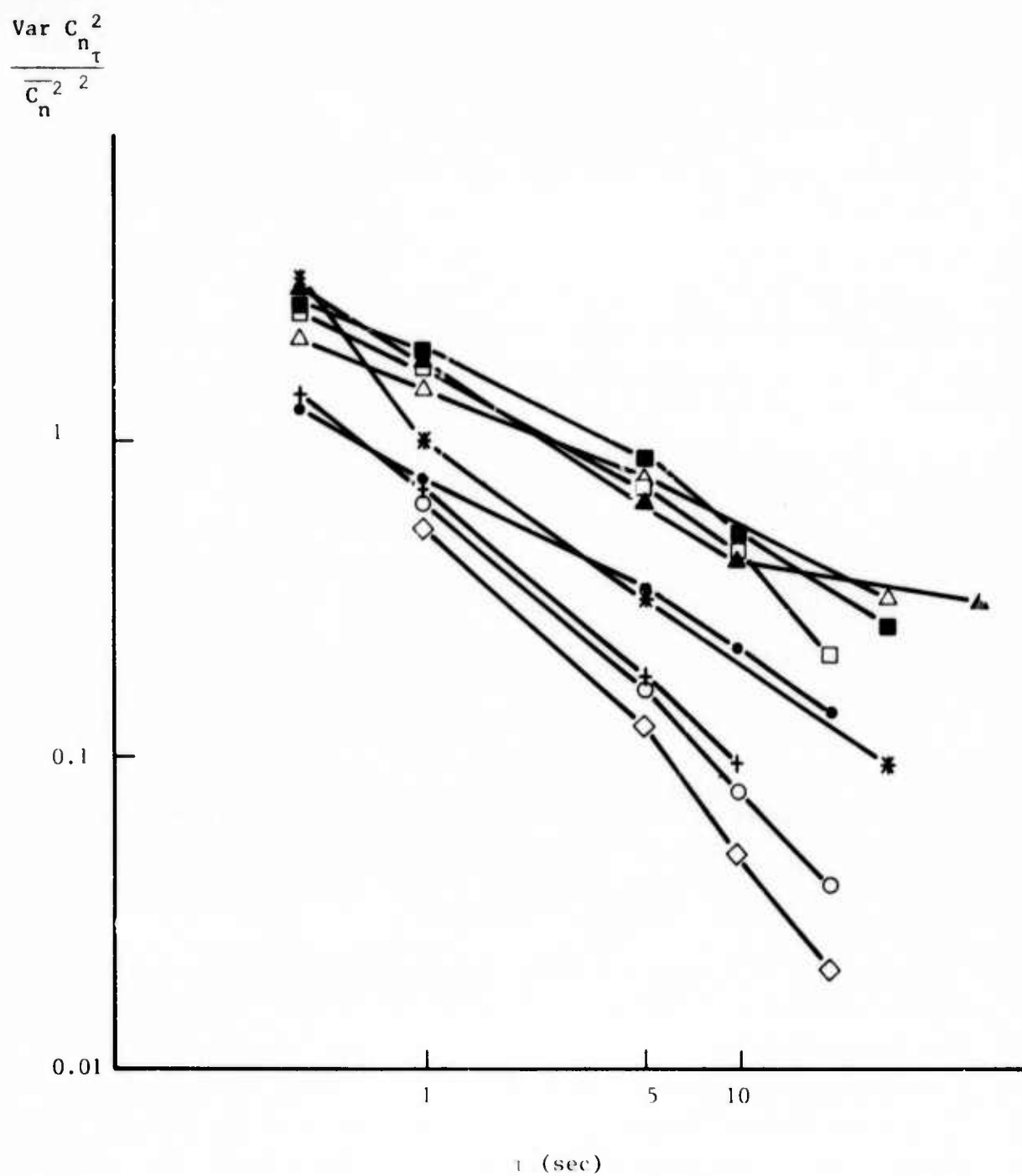


Figure 2a. Normalized variance (spread) of measurements of strength of microthermal and optical fluctuations, vs. averaging time ( $\tau$ ). Microthermal case ( $C_n^2$ ).



$$\frac{\text{Var } \sigma_{\tau}^2}{\sigma^2}$$

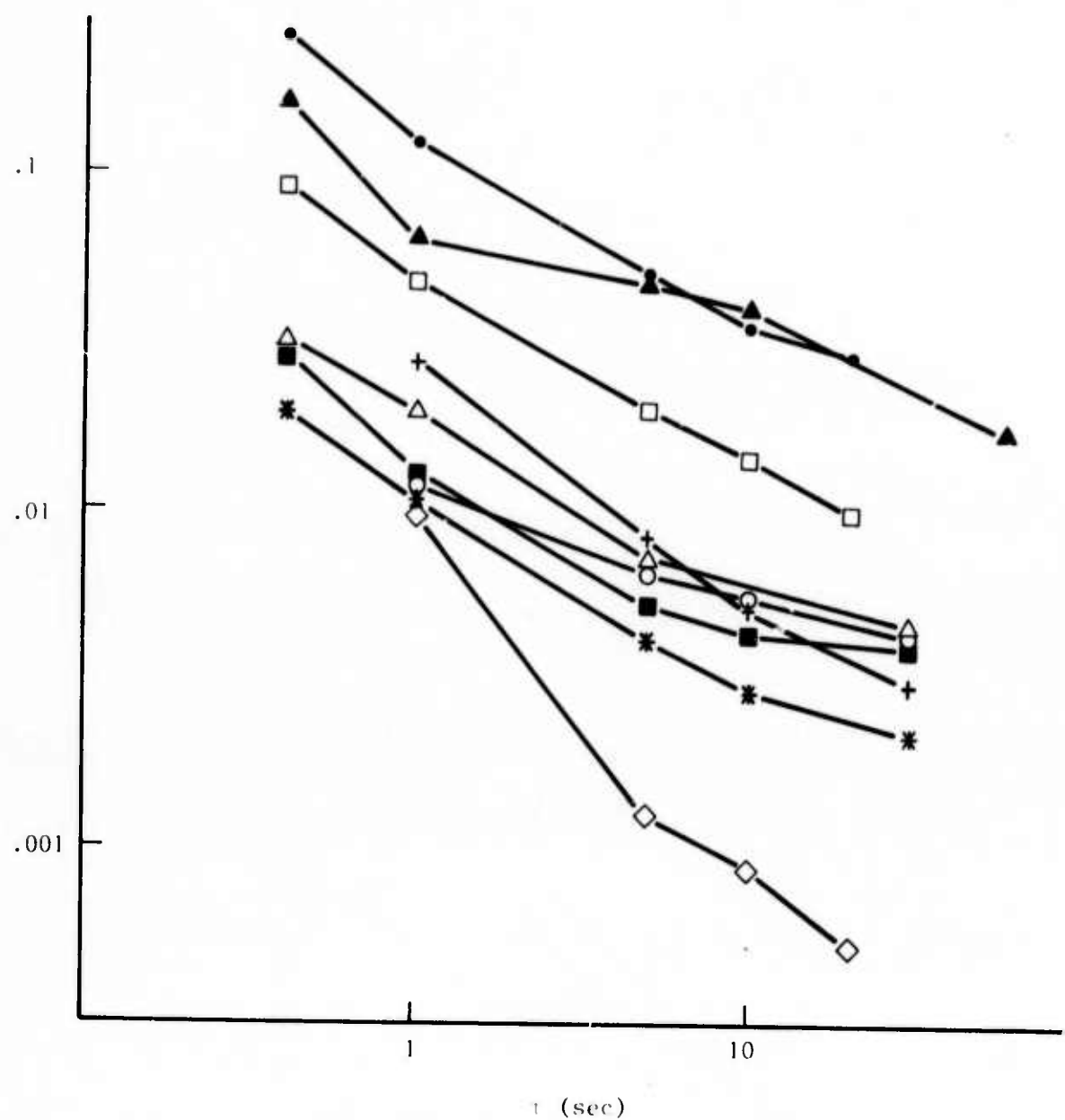


Figure 2b. Normalized variance (spread) of measurements of strength of microthermal and optical fluctuations, vs. averaging time ( $\tau$ ). Optical (log amplitude) scintillations ( $\sigma_{\tau}^2$ ).



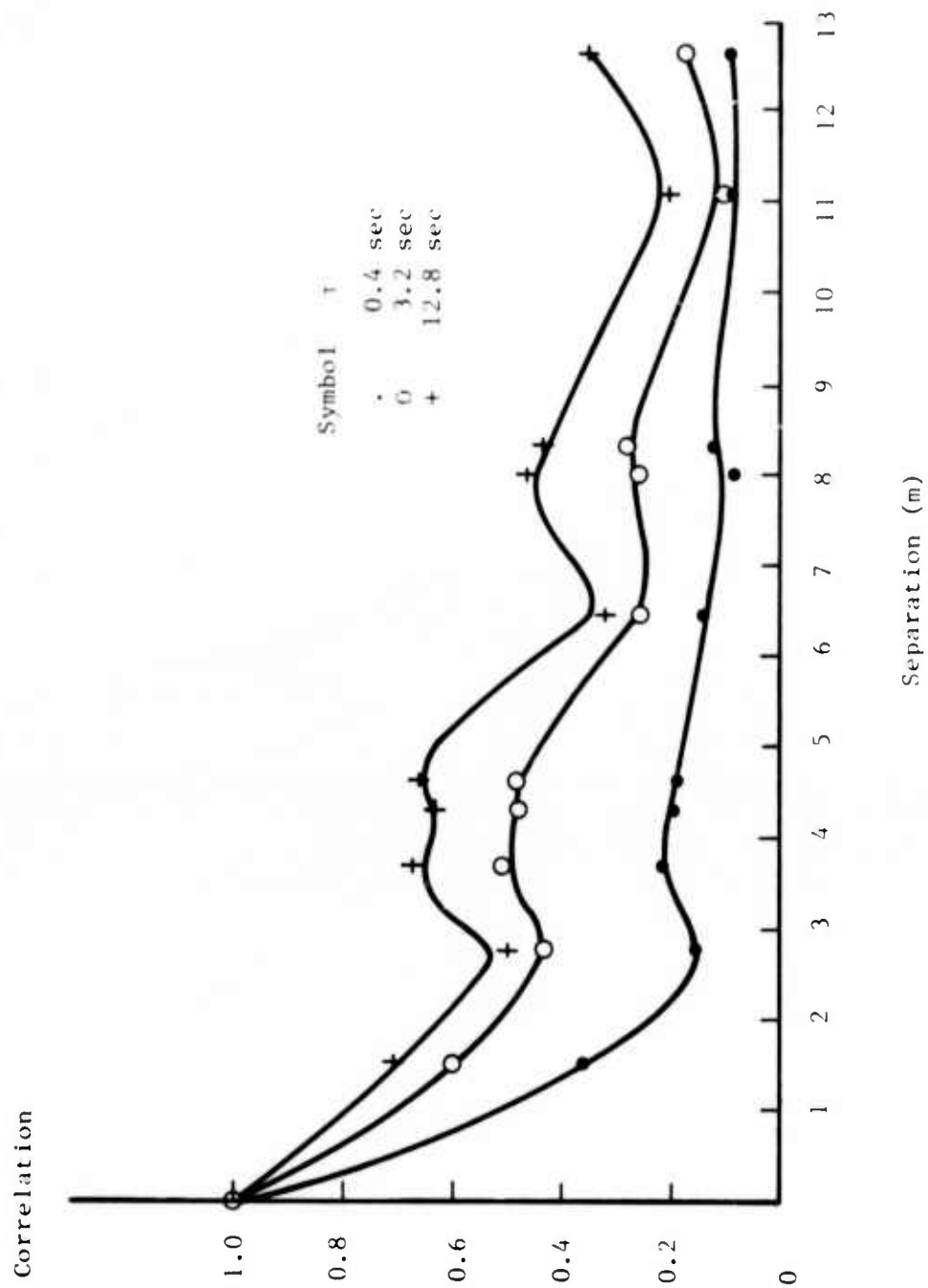


Figure 3a. Microthermal-envelope or strength-of-turbulence spatial correlations vs. separation in a direction parallel to the wind, for three values of averaging time ( $\tau$ ). Wind speed 1.5 m/sec.



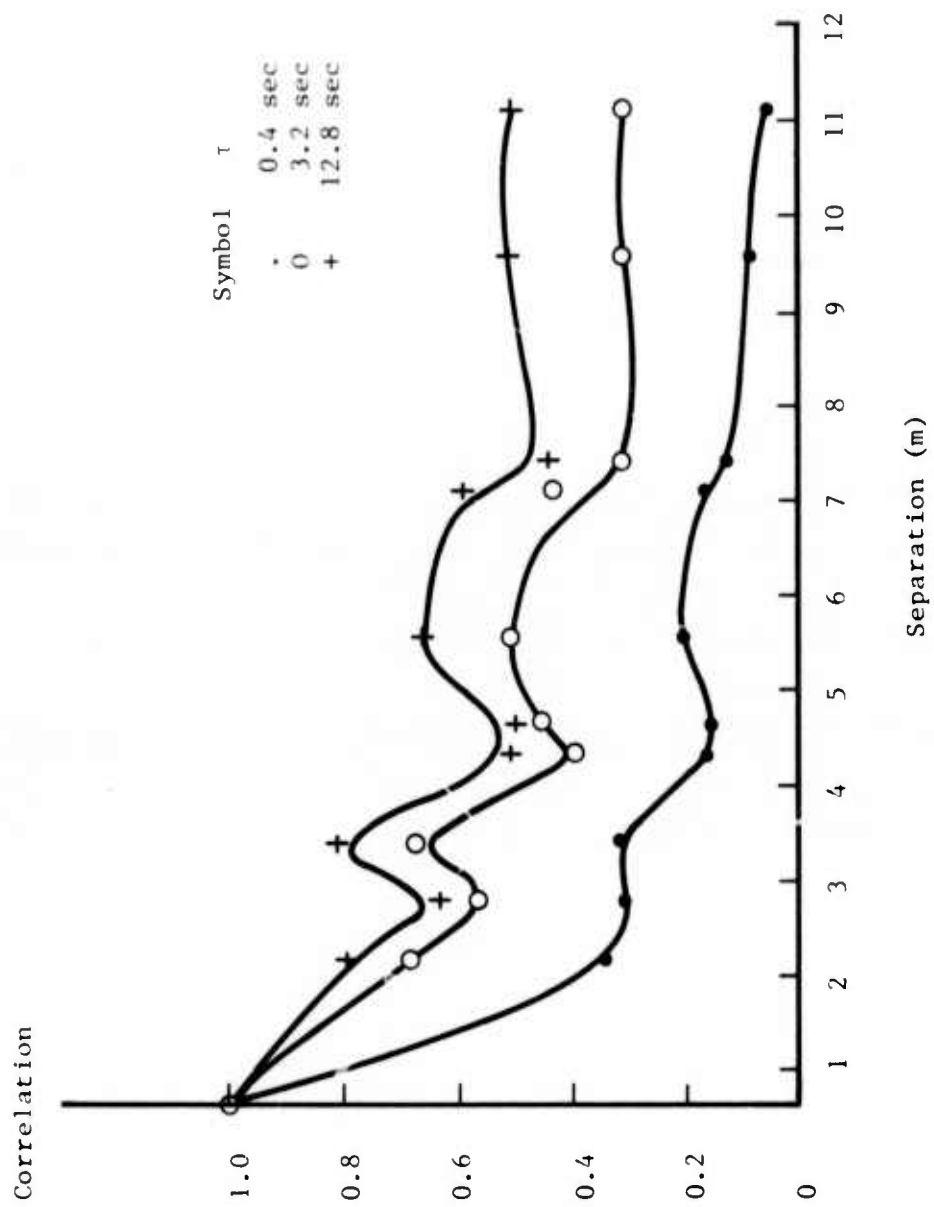


Figure 3b. Microthermal-envelope or strength-of-turbulence spatial correlations vs. separation in a direction parallel to the wind, for three values of averaging time ( $\tau$ ).  
Wind speed 4.6 m/sec.



Similar curves for a transverse wind are given in Figs. 4a, b. The tendency for the large- $\tau$  curve to decorrelate at larger separations is evident in Fig. 4b. In Fig. 4a, an anomaly is observed whereby the basic squared-microthermal-fluctuations exhibit a correlation tail at large separations, which is also manifested in the large- $\tau$  case.

### C. A Quantitative View of Turbulence Intermittency

A simple operational measure of the "intermittency" of turbulence is

$$R = \frac{\text{Standard Deviation for } C_n^2}{C_n^2}, \quad (5)$$

where  $\tau$  may be taken as e.g. 10 seconds. In Figure 5 we show differential probe measurements of  $\Delta T$  for values of  $R$  of 0.46 and 0.68, which might be described as intermediate and pronounced intermittency, respectively.

In Table II, data ranging from cases of light intermittency ( $R = 0.26$ ) to heavy intermittency ( $R = 0.77$ ) are shown. The integral scale of  $\Delta T^2$  after filtering or smoothing with  $\tau = 1$  sec, is the integral of the autocorrelation function of this smoothed process; it is seen to increase with increased intermittency, as expected, and decreases toward  $\tau/2$  only for light intermittency. This indicates that intermittency does indeed introduce a long tail in the correlation function of the basic, unfiltered ( $\Delta T^2$ ) process. Similarly, the flatness factor  $\beta_2$  (Ref. 1) associated with the probability distribution of the unfiltered fluctuations is seen to be much higher in the intermittent case, directly indicating the predominance of occasional excursions of extreme magnitude in that case. It may be also noted that intermittency is generally associated with low-wind, poorly-mixed conditions characterized by occasional "bursts" of turbulence.



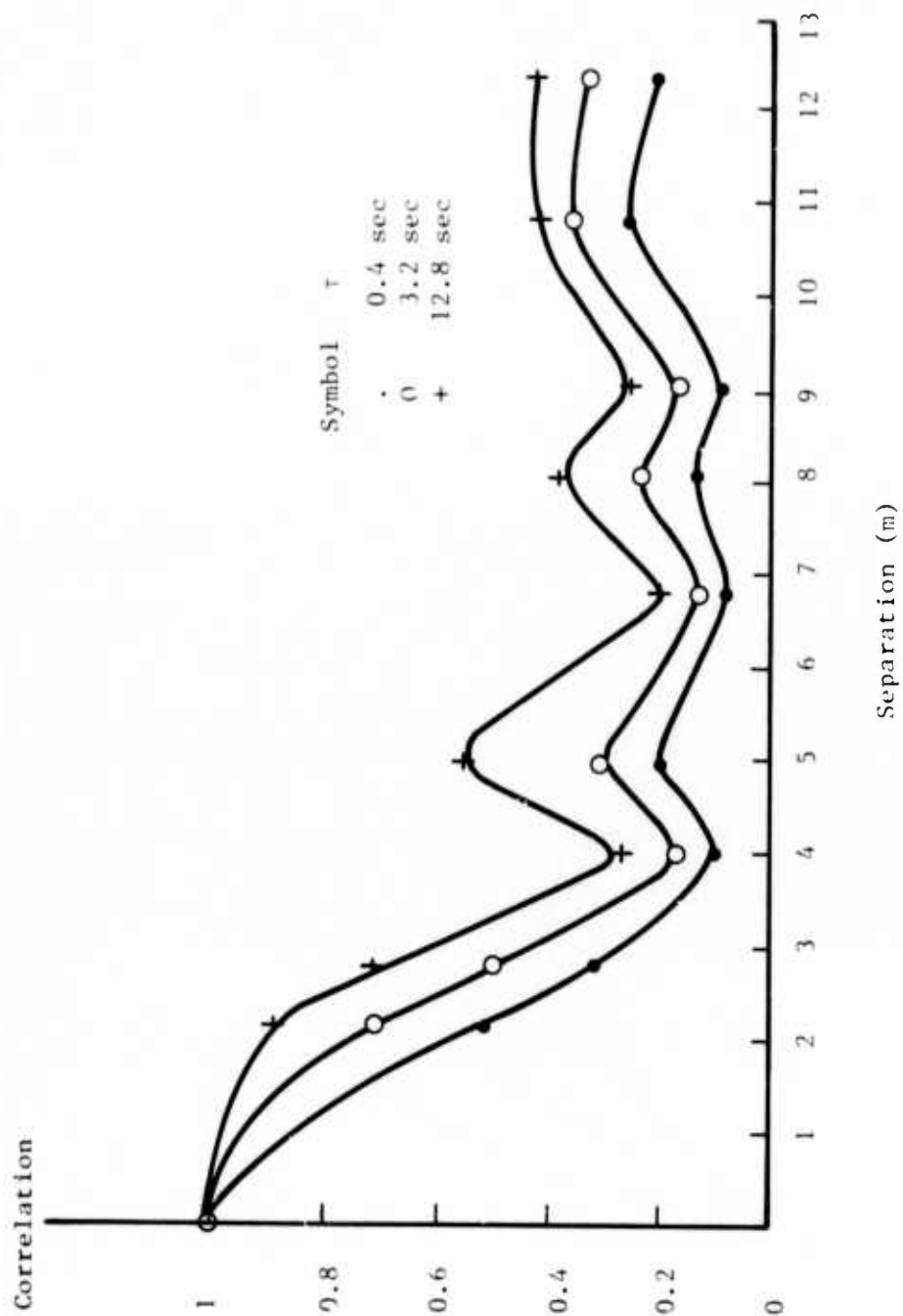


Figure 4a. Microthermal-envelope or strength-of-turbulence spatial correlations vs. separation in a direction perpendicular to the wind, for three values of averaging time ( $\tau$ ).  
Wind speed 0.91 m/sec.



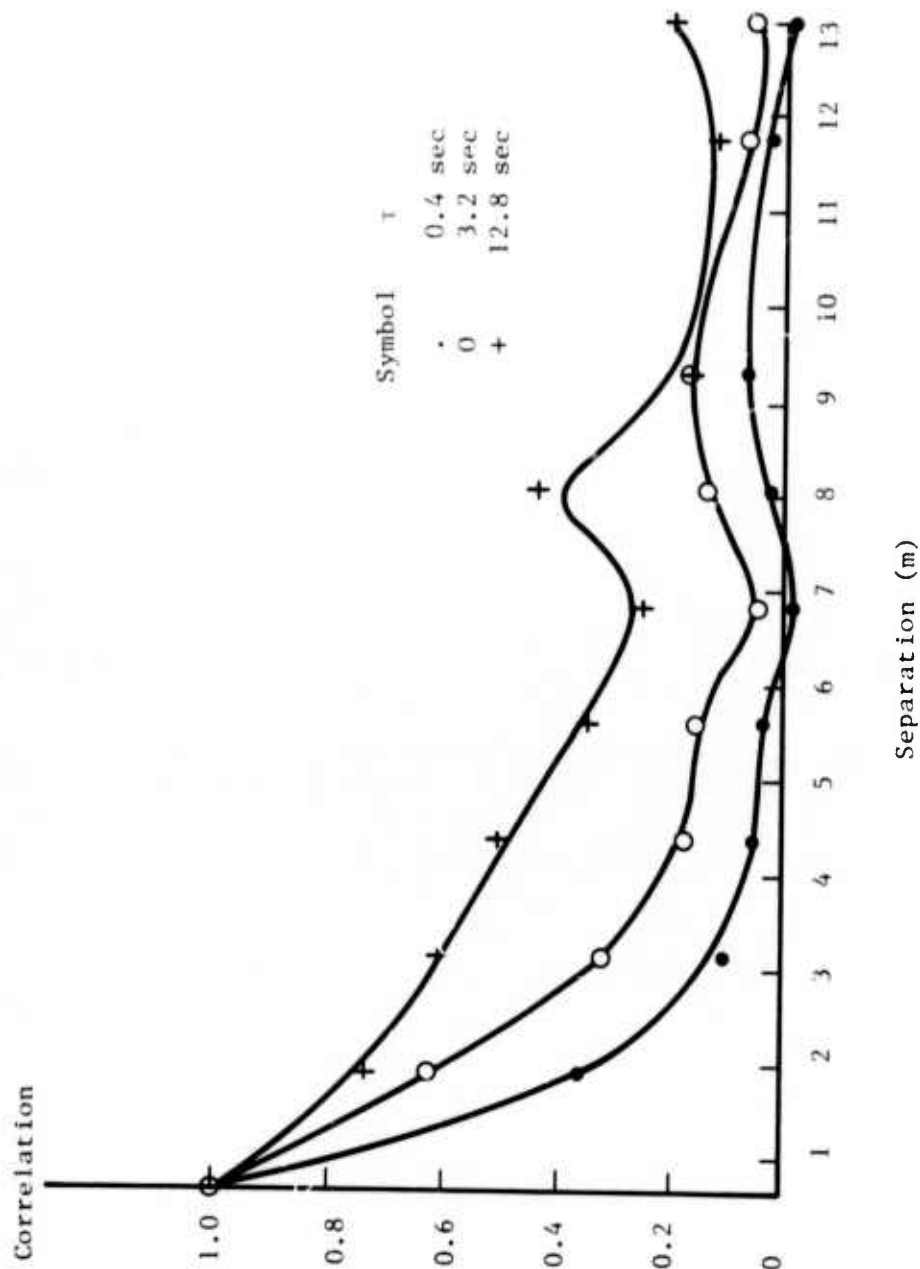


Figure 4b. Microthermal-envelope or strength-of-turbulence spatial correlations vs. separation in a direction perpendicular to the wind, for three values of averaging time ( $\tau$ ).  
Wind speed 1.5 m/sec.



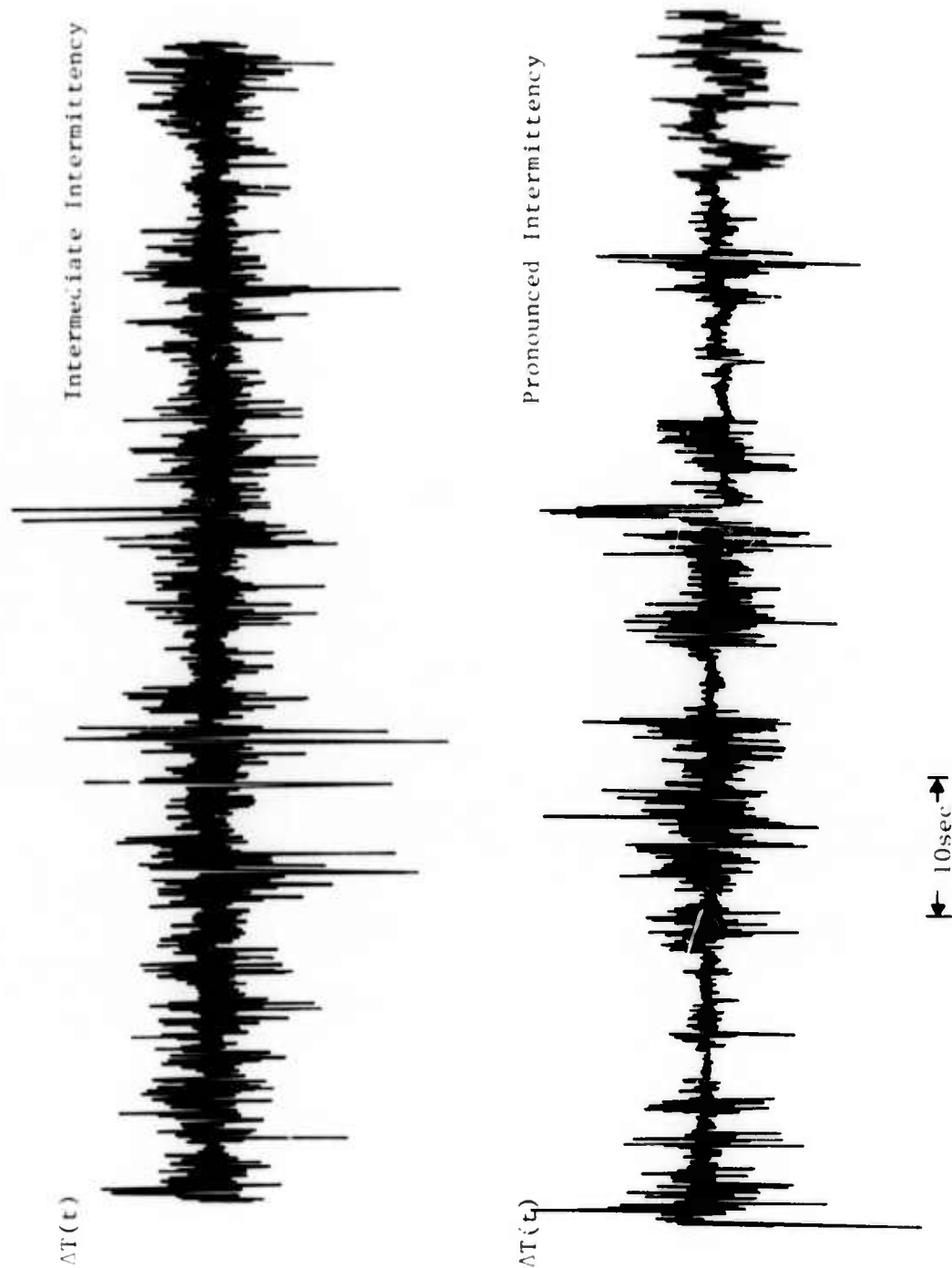


Figure 5. Differential probe measurements of microthermal fluctuations  $\Delta T(t)$ , indicating conditions of intermediate and pronounced intermittency of turbulence.



TABLE I.

| Wind Speed (v) | S.D. $C_n^2 = 10 \text{ sec.}$ |         | Int. Scale<br>$\Delta T^2$<br>$\tau = 1 \text{ sec}$ | Corr.<br>Length<br>$v \cdot I_{\Delta T^2}$ | $\beta_2$<br>$\Delta T$ |
|----------------|--------------------------------|---------|--|---|-------------------------|
|                | $R = \frac{C_n^2}{C_n^2}$      | $C_n^2$ |  |   |                         |
| (m/sec)        |                                |         | (sec)  | (m)   |                         |
| 9              |                                | .270    | 0.8  | 7.2   | 5.5                     |
| 5.5            |                                | .261    | 1.38   | 7.6   | 8.35                    |
| 4.5            |                                | .457    | 1.47   | 6.6   | 11.15                   |
| 3.8            |                                | .468    | 1.49   | 5.7   | 13.4                    |
| 1.5            |                                | .767    | 3.48   | 5.2   | 12.32                   |



### III. CONDITIONAL FADING STATISTICS

A topic related to the short-term considerations discussed previously is that of the conditional statistics of scintillation or irradiance fluctuations. The applications of this concept include "pilot-tone" or burst communications systems in which the channel is monitored and used only when it is "good", and target illumination systems in which e.g. a high-power laser is utilized immediately after a low-power laser (or some other channel monitoring scheme) indicates a favorable short-term path. The applicable question may be posed as follows: given that the instantaneous target irradiance is above some predetermined threshold, what is the probability distribution of the irradiance at an arbitrary time  $\tau$  later? The present discussion is limited to the linear propagation case.

#### A. Analysis of the Conditional Problem

In previous work on this program, it has been determined that scintillation does not constitute a Markov process. It has been determined by ourselves and a number of other investigators, however, that this phenomenon is for most practical purposes log-normally-distributed. To the extent that we can assume that the two-point log distribution is bivariate normal, the problem is readily tractable.<sup>2</sup> However, we point out that the conditional statistics can be very sensitive to departures from this distribution and theoretical arguments suggest that exact log normality is not even possible for the one-point distribution.<sup>3</sup> Furthermore, as described below, our preliminary analysis of experimental data shows significant departure of the two-point distribution from the normal under conditions of strong scintillation.

Nevertheless, the basic approach given here to the conditional problem can be numerically extended to utilize any (non-gaussian) joint

- 
2. S. O. Rice, "Mathematical Analysis of Random Noise", in Selected Papers on Noise and Stochastic Processes, N. Wax., ed., Dover Publications, Inc., N.Y., 1954.
  3. J. W. Strohbehn, T. Wang, J. P. Speck, Radio Science 10, 59-70, January 1975.



probability distribution which may be empirically or otherwise determined. We will confine this discussion to the log-normal case for simplicity, and empirical verification under certain conditions will be given below.

Let us therefore assume that the two-point or joint probability distribution of the log irradiance is bivariate normal. The important parameter is the correlation coefficient  $\rho(\tau)$ , which is a function of the time delay  $\tau$  separating the initial and final observations of the irradiance. The joint distribution of the log irradiance  $\chi$  is

$$\Pr(\chi(t), \chi(t + \tau)) = \frac{1}{2\pi\sigma_0^2(1-\rho^2(\tau))^{1/2}} \exp \left\{ -\frac{1}{2\sigma_0^2(1-\rho^2(\tau))} \cdot (\chi^2(t) - 2\rho(\tau)\chi(t)\chi(t + \tau) + \chi^2(t + \tau)) \right\} \quad (6)$$

where  $\chi$  is normally distributed with variance  $\sigma_0^2$  and zero mean, and

$$\rho(\tau) \equiv \frac{\langle \chi(t)\chi(t + \tau) \rangle}{\sigma_0^2}$$

The conditional distribution of  $\chi(t + \tau)$ , given that  $\chi(t) = L$ , is

$$\Pr(\chi(t + \tau) | \chi(t) = L) = \frac{1}{\sqrt{2\pi}\sigma_0(1-\rho^2(\tau))^{1/2}} \exp \left\{ \frac{-1}{2\sigma_0^2(1-\rho^2(\tau))} \cdot (\chi(t + \tau) - \rho(\tau)L)^2 \right\} \quad (7)$$



which is normal with the following mean and variance:

$$\begin{aligned}\text{Mean} &= L\rho(\tau) \\ \text{Var} &= \sigma_0^2 (1-\rho^2(\tau))\end{aligned}\quad (8)$$

We are now interested in the probability that  $\chi(t + \tau)$  is less than a fixed "fade" level ( $\ell_1$ ), given that  $\chi(t)$  exceeds a threshold "pilot level" ( $\ell_0$ ):

$$\begin{aligned}\Pr(\chi(t + \tau) \leq \ell_1 \mid \chi(t) \geq \ell_0) &= \int_{\ell_0}^{\infty} d\chi(t) \int_{-\infty}^{\ell_1} d(\chi(t + \tau)) P(\chi(t), \chi(t + \tau)) \\ &= \int_{\ell_0}^{\infty} d\chi \frac{1}{\sigma\sqrt{2\pi}} e^{\frac{-\chi^2}{2\sigma^2}}\end{aligned}\quad (9)$$

We define the following quantities:<sup>4</sup>

$$Z(x) \equiv \frac{1}{\sqrt{2\pi}} e^{-x^2/2} \quad (9a)$$

$$P(x) \equiv \int_{-\infty}^x Z(t)dt \quad (9b)$$

$$Q(x) \equiv \int_x^{\infty} Z(t)dt \quad (9c)$$

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4. M. Abramowitz and I. Stegun, ed., Handbook of Mathematical Functions, Dover Publications, Inc., N.Y. 931-940, 1965.



$$g(x,y,\rho) = (2\pi\sqrt{1-\rho^2})^{-1} \exp \left[ -\frac{1}{2(1-\rho^2)} (x^2 - 2\rho xy + y^2) \right] \quad (9d)$$

$$L(h,k,\rho) = \int_h^\infty dx \int_k^\infty dy g(x,y,\rho) \quad (9e)$$

We note that

$$P(x) + Q(x) = 1 \quad (10a)$$

$$P(-x) = Q(x) \quad (10b)$$

$$L(h,-k,-\rho) = \int_h^\infty dx \int_{-\infty}^k dy g(x,y,\rho) \quad (10c)$$

With these definitions, we have

$$\begin{aligned} \Pr(\chi(t + \tau) \leq \ell_1 | \chi(t) \geq \ell_0) &= L\left(\frac{\ell_0}{\sigma_0}, \frac{-\ell_1}{\sigma_0}, -\rho\right) / Q\left(\frac{\ell_0}{\sigma_0}\right) \\ &= L\left(\frac{\ell_0}{\sigma_0}, \frac{-\ell_1}{\sigma_0}, -\rho\right) / P\left(\frac{-\ell_0}{\sigma_0}\right) \end{aligned} \quad (11)$$

This expression must be evaluated numerically for various values of  $\ell_0$ ,  $\ell_1$ ,  $\sigma_0$ , and  $\rho$ . The calculation is expedited by use of the formula



$$L(h, k, \rho) = Q(h)Q(k) + \sum_{\eta=0}^{\infty} \frac{Z^{(\eta)}(h)Z^{(\eta)}(k)}{(\eta+1)!} \rho^{\eta+1} \quad (12)$$

where

$$Z^{(\eta)}(x) = \frac{d^{\eta}}{dx^{\eta}} Z(x) = -xZ^{(\eta-1)}(x) - (\eta-1)Z^{(\eta-2)}(x) \quad (13)$$

In practice, in the worst cases about 50 terms must be retained in the sum for the accuracy to be better than  $1 \times 10^{-6}$ .

We have performed computer runs for several different pilot and fade levels, using correlation functions (Fig. 6,6a) obtained empirically under three different scintillation conditions at  $10.6\mu$ :

|       | <u>Strength of Scintillation</u> | <u>Wind Speed</u>             | <u>Symbol</u> |
|-------|----------------------------------|-------------------------------|---------------|
| Run A | $\sigma_0^2/4 = 0.307$           | 1 m/s variable                | A             |
| Run B | $\sigma_0^2/4 = 0.010$           | 3.5 m/s at $45^\circ$ to path | $\emptyset$   |
| Run C | $\sigma_0^2/4 = 0.0015$          | 9 m/s at $45^\circ$ to path   | X             |

The pilot and fade levels are conveniently normalized by the mean irradiance  $\bar{I}$ . We thus calculate the probability that  $\ln [I(\tau)/\bar{I}] \leq \ln(I_1/\bar{I})$  given that  $\ln [I(0)/\bar{I}] \geq \ln(I_0/\bar{I})$ , for particular correlation functions and values of  $\sigma_0^2$ ,  $I_1$ ,  $I_0$ .

The results for strong scintillations (Run A), a fade level of  $0.5 \bar{I}$ , and six pilot levels are shown in Fig. 7. It is apparent that, for this particular correlation function, indicative of a low wind condition and strong scintillation, a conditioning or pilot threshold of  $0.95 \bar{I}$  results in a less than 5% probability that the irradiance will fall below  $0.5 \bar{I}$  until 18 msec later. If the conditioning threshold is



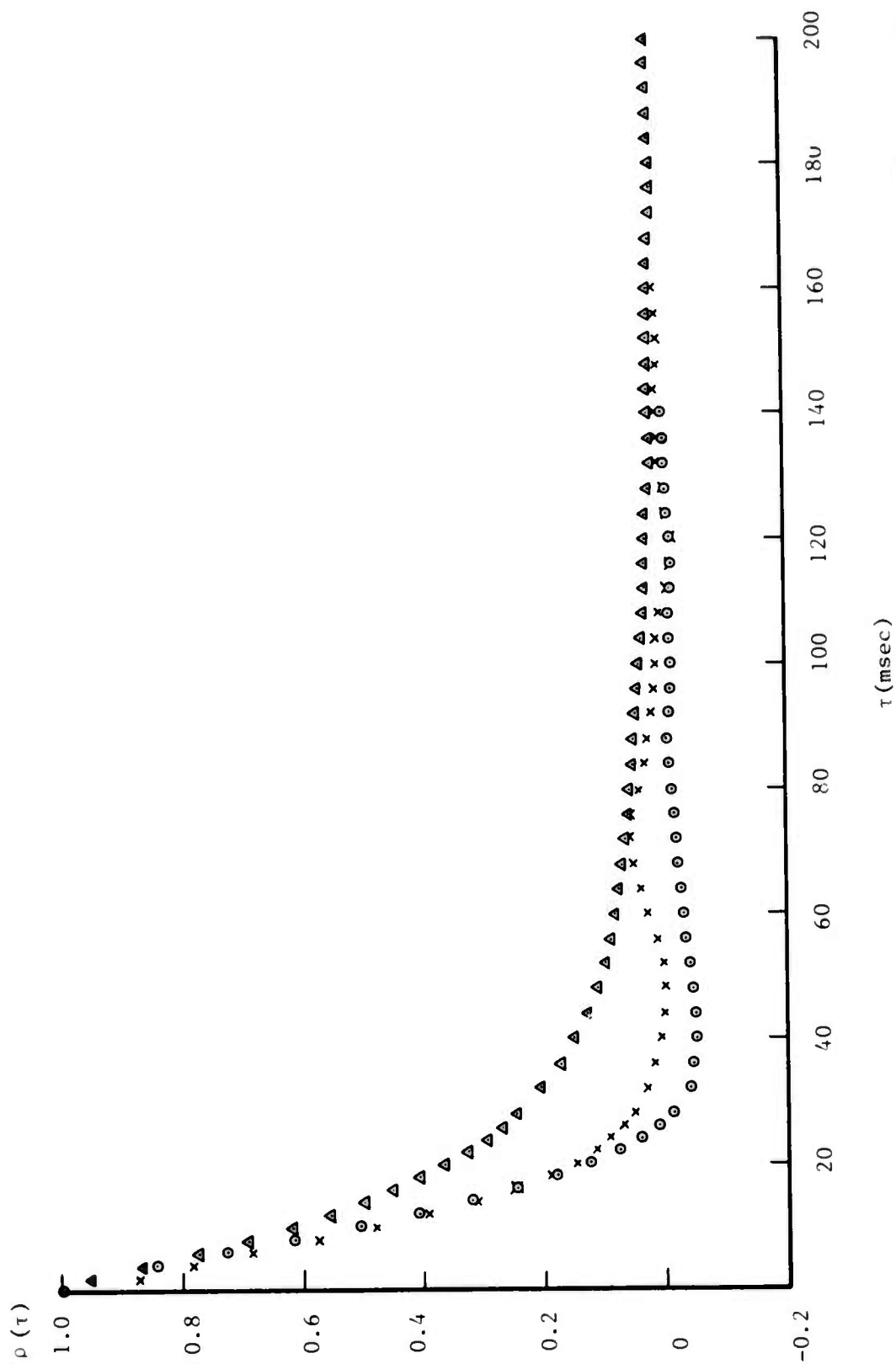


Figure 6. Empirical, two-point temporal correlation functions ( $\rho$ ) for log irradiance scintillations, vs. delay time ( $\tau$ ).



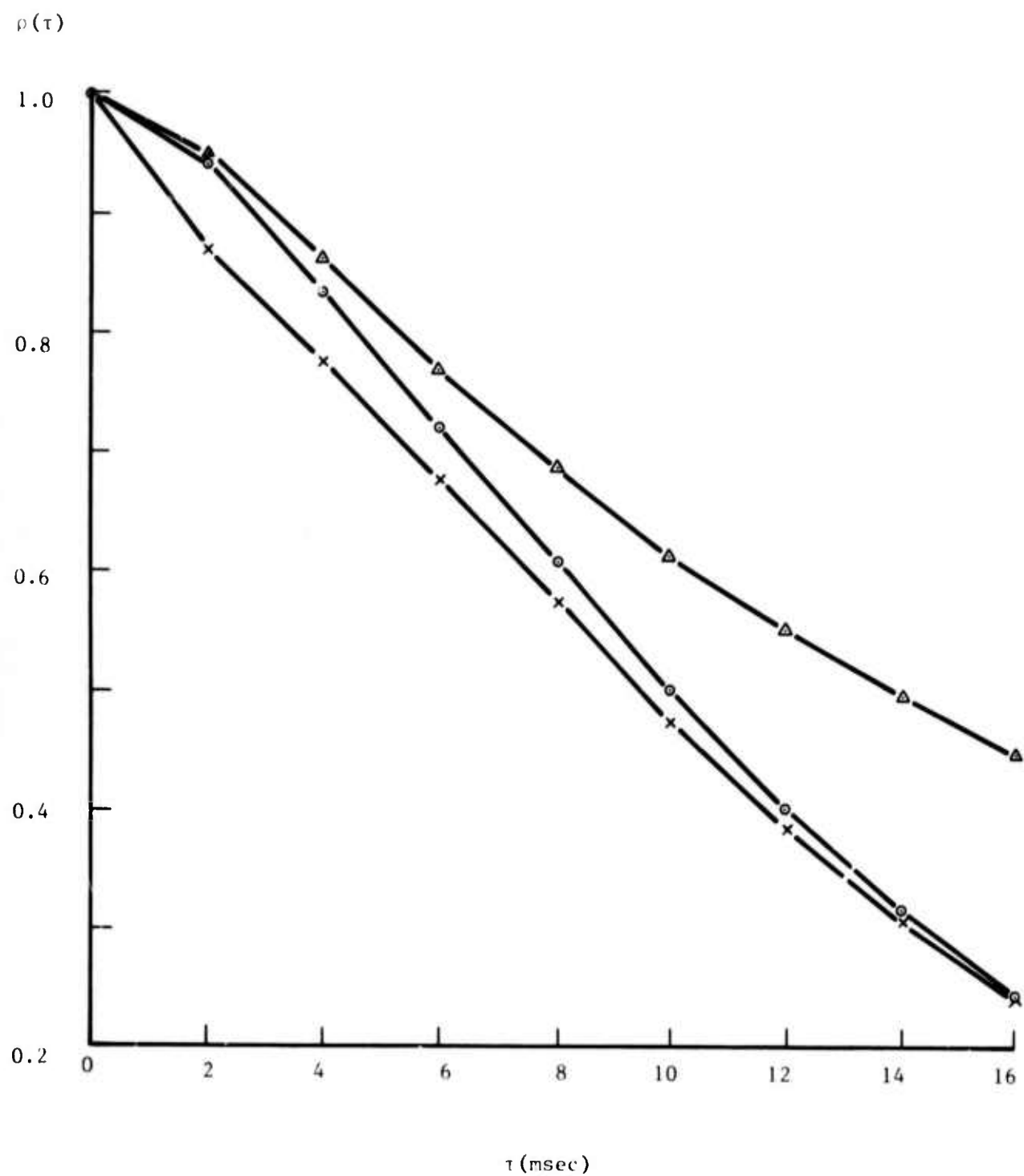


Figure 6a. Expanded detail for Fig. 6 at small delays ( $\tau$ ).



Probability  $\frac{I(\tau)}{I} \leq 0.5$

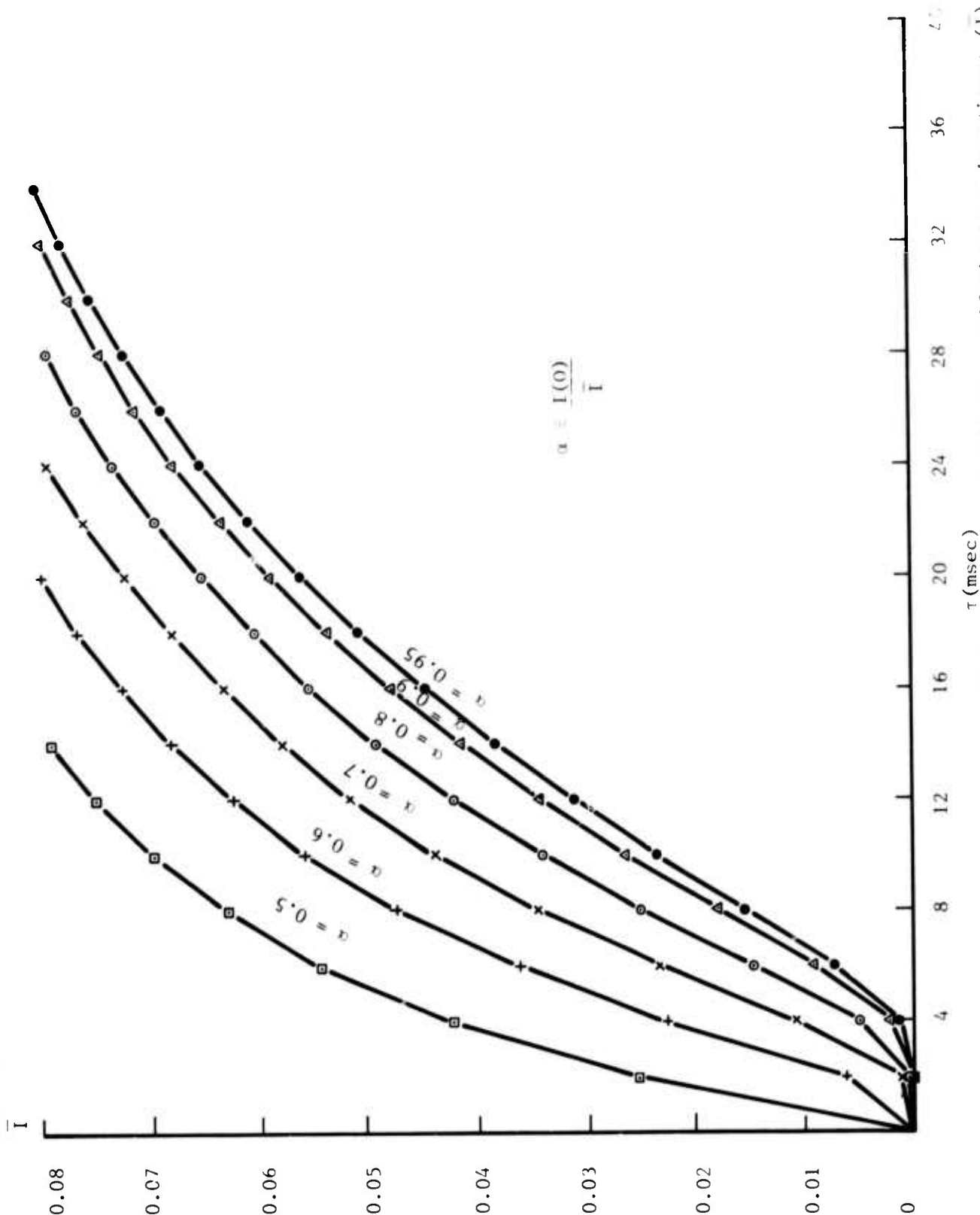


Figure 7. The probability that irradiance  $I(\tau)$  at time  $t = \tau$  will be  $\leq$  half the mean irradiance  $(\bar{I})$ , given that it is  $\geq \alpha \bar{I}$  at  $t = 0$ , vs.  $\tau$  (Run A). Six values of the parameter  $\alpha$  are shown.



0.5  $\bar{I}$ , the corresponding time interval is 5 msec. As the threshold is made lower, it will be reached more often, but the following time interval for favorable propagation conditions will be correspondingly shorter. For instance, for a threshold of 0.7  $\bar{I}$ , which is exceeded 74% of the time, and a time interval of 1 msec, the fade level will fall below 0.5  $\bar{I}$  only once in 1,000 times. This approach obviously yields sufficient information for an analysis of use-rate vs. reliability.

#### B. Test of the Bivariate Normal Distribution

The degree to which the empirical scintillation data agree with the above assumption of two-point bivariate normality for the log irradiance is being investigated for a number of runs. For example, for the weak scintillation case of Run C, the one-point log distribution (Fig. 8) has an observed skewness of 0.05 and kurtosis of 3.1. Table III shows the skewness and kurtosis of the conditional distributions vs.  $\tau$  and the pilot level  $\ell_0$ , where  $\chi$  and  $\ell_0$  have been normalized by the standard deviation  $\sigma_0$ . The distributions indicate normality except for small  $\tau$  and  $\frac{\ell_0}{\sigma_0} = -1$ . Three of these conditional distributions are shown in Fig. 9.

Using measured values of the correlation function for this run (Table IV), we compare the predicted, normalized conditional mean and variance (Eq. 8) with observed values, in Tables V and VI. Excellent agreement with the gaussian assumption is evident.

Under conditions of strong scintillation, e.g. Run A above, there is evidence of appreciable departure from the bivariate normal distribution. This is under further investigation.

### IV. NEW EXPERIMENTAL WORK AND FACILITIES

#### A. Target Irradiance Statistics with Beam Wander Cancellation

In preceding reports on this program (Refs. 1,5), analytical results were given for the mean target irradiance and its fluctuations resulting from the effects of turbulence on a finite beam wave, including the cancellation of turbulence-induced beam wander. Experimental results were given for a 1.6 km path operating at 6328 $\text{\AA}$  with a wander-cancelling tracker.



Probability (%)

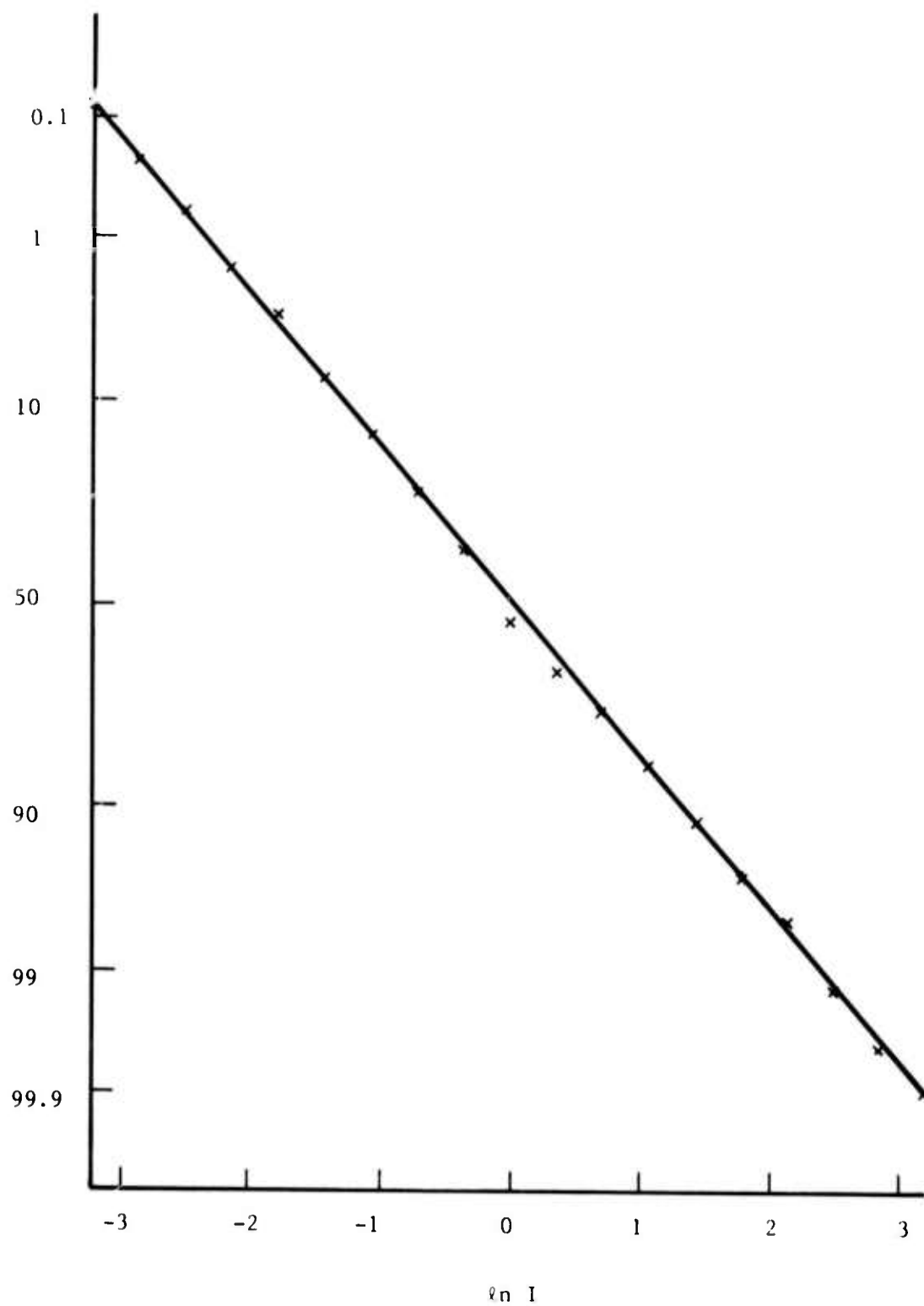


Figure 8. One-point probability distribution of log irradiance for Run C.



TABLE III

Skewness (S) and Kurtosis (K) of  $\text{Pr}(\chi(t + \tau) | \chi(t))$  for Run C

| S  |        |       |       |        |       |
|--|--------|-------|-------|--------|-------|
| $\frac{\ell_0}{\sigma_0} \backslash \tau \text{ (ms)}$ | 1      | 2     | 4     | 8      | 16    |
| -1   | .29    | .13   | .2    | .022   | .012  |
| 0  | .03    | .051  | .056  | .061   | .068  |
| 1  | -.12   | -.017 | .01   | .13    | -.055 |
| 2  | -.0039 | .047  | .0080 | -.0065 | -.036 |

| K  |      |      |       |      |      |
|--|------|------|-------|------|------|
| $\frac{\ell_0}{\sigma_0} \backslash \tau \text{ (ms)}$ | 1    | 2    | 4     | 8    | 16   |
| -1   | 4.2  | 3.59 | 3.83  | 3.29 | 3.18 |
| 0  | 3.20 | 3.16 | 3.089 | 3.05 | 3.04 |
| 1  | 3.27 | 3.21 | 2.69  | 2.77 | 3.17 |
| 2  | 2.83 | 2.84 | 2.95  | 2.98 | 3.08 |



Conditional Probability (%)

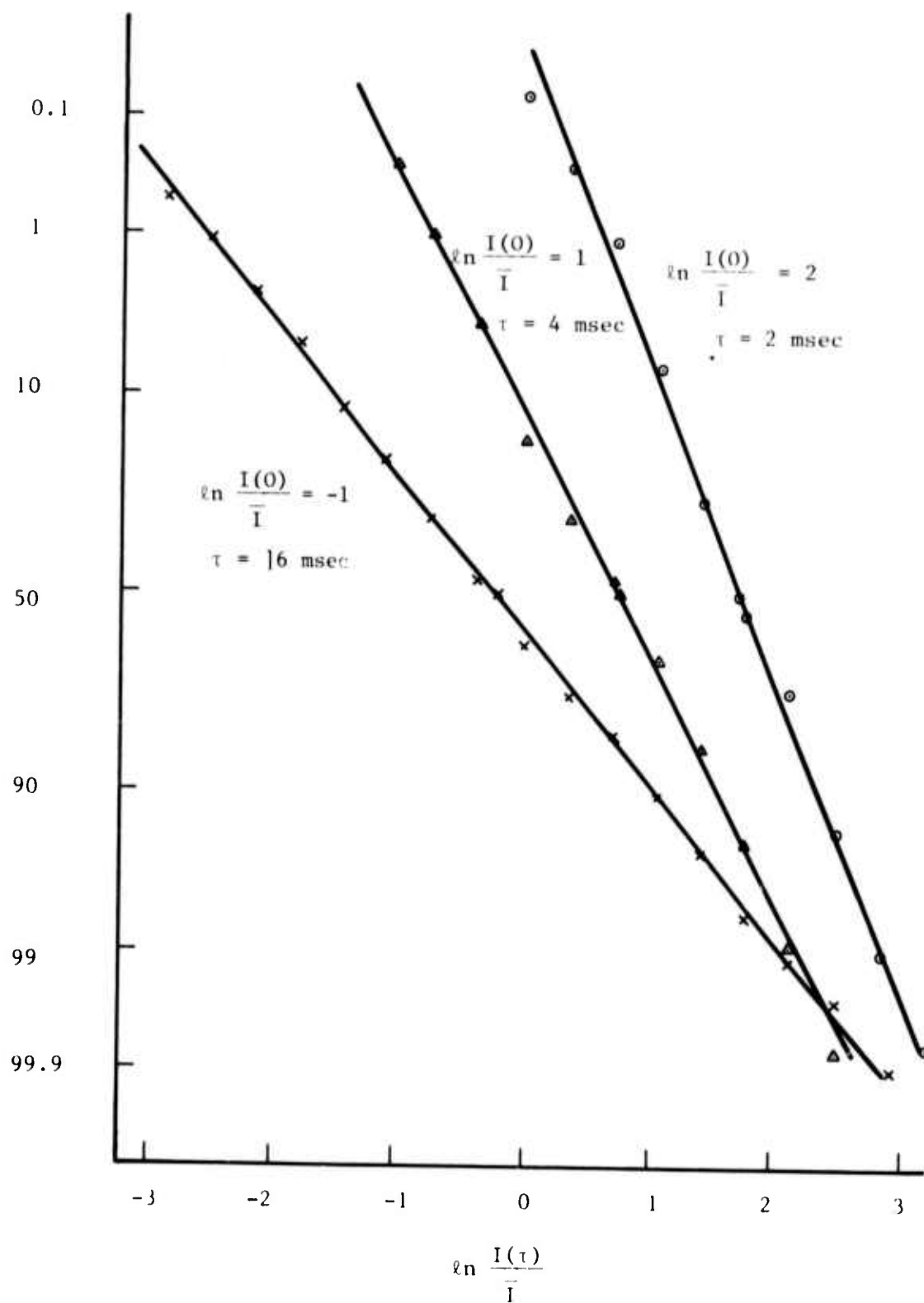


Figure 9. Conditional probability for normalized log irradiance at time  $t = \tau$ , given the value at  $t = 0$ .



TABLE IV

Correlation Function Values for Run C

| $\tau$ | $\rho(\tau)$ |
|--------|--------------|
| 2 ms   | 0.87         |
| 4 ms   | 0.78         |
| 8 ms   | 0.57         |
| 16 ms  | 0.24         |

TABLE V

Comparison of Predicted and Observed Mean of  $\Pr\left(\frac{\chi(t+\tau)}{\sigma_0} \middle| \frac{\chi(t)}{\sigma_0} = \frac{\ell_0}{\sigma_0}\right)$   
 For Run C

| $\frac{\ell_0}{\sigma_0} \backslash \tau \text{ ms}$ | 2      | 4      | 8      | 16    |
|--|--------|--------|--------|-------|
| -1 Predicted   | -0.87  | -0.78  | -0.57  | -0.24 |
| Observed   | -0.89  | -0.75  | -0.60  | -0.24 |
| 0 Predicted  | 0      | 0      | 0      | 0     |
| Observed   | -0.016 | -0.016 | -0.001 | 0.008 |
| 1 Predicted  | 0.87   | 0.78   | 0.57   | 0.24  |
| Observed   | 0.85   | 0.72   | 0.50   | 0.21  |
| 2 Predicted  | 1.74   | 1.56   | 1.14   | 0.48  |
| Observed   | 1.70   | 1.51   | 1.09   | 0.45  |



TABLE VI

Comparison of Predicted and Observed  $\frac{\text{Variance}}{\sigma_o^2}$  of  $\Pr\left(\frac{\chi(t + \tau)}{\sigma_o} \middle| \frac{\chi(t)}{\sigma_o} = \frac{\ell_o}{\sigma_o}\right)$   
 For Run C

| $\frac{\ell_o}{\sigma_o} \backslash \tau \text{ ms}$ | 2     | 4     | 8     | 16    |
|--|-------|-------|-------|-------|
| -1 Predicted   | 0.243 | 0.392 | 0.675 | 0.942 |
| Observed   | 0.239 | 0.414 | 0.651 | 0.936 |
| 0 Predicted  | 0.243 | 0.392 | 0.675 | 0.942 |
| Observed   | 0.236 | 0.406 | 0.686 | 0.961 |
| 1 Predicted  | 0.243 | 0.392 | 0.675 | 0.942 |
| Observed   | 0.278 | 0.402 | 0.77  | 1.01  |
| 2 Predicted  | 0.243 | 0.392 | 0.675 | 0.942 |
| Observed   | 0.254 | 0.439 | 0.765 | 0.99  |



Following the above experimental effort, the facility was modified for taking similar data over a much shorter path. This was done in order to achieve smaller ratios of transmitter-diameter-to-coherence-scale ( $D/\rho_0$ ) for stronger, reasonably developed turbulence, while maintaining a sufficient Fresnel number for the transmitter. This case scales to the infrared conditions of interest, and experiments with this facility have been underway for several months.

The facility is currently undergoing a further modification, to add a simultaneous, coincident-beam capability at  $10.6\mu$ . The tracker continues to operate off a target-point beacon at  $6328\text{\AA}$ , but will now control both optical and  $10\mu$  beams (Fig. 10). It is expected that the turbulence-induced wander, being a basically geometrical-optics phenomenon,<sup>5</sup> will not undergo significant wavelength dispersion, so that this tracking scheme will effectively remove wander at the infrared wavelength. Operation at  $10.6\mu$  will afford a wavelength-scaled test of our analytical results, and will further reduce  $D/\rho_0$  in a well developed turbulence. The receiver configuration is shown in Fig. 11, and in the photograph of Fig. 12.

The data capability and experimental parameters of this enlarged system are summarized in Table VII. We also mention that the analysis given in the preceding report,<sup>1</sup> for the on-axis mean irradiance in the limit  $\frac{D}{\rho_0} \rightarrow \infty$ , is being extended to include some details of the complete curve  $\left(1 \ll \frac{D}{\rho_0} < \infty\right)$ . This is being accomplished by means of the extended Huygens-Fresnel formulation and an asymptotic expansion in inverse powers of  $D/\rho_0$ . This approach is free of the assumptions and approximations of a recent Russian treatment.<sup>6</sup>

#### B. Long-Path Saturation System

In earlier work on this program,<sup>7</sup> experiments were conducted over the longest, lowest path which can be reasonably achieved in the

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5. J. R. Kerr and J. R. Dunphy, "Propagation of Multiwavelength Laser Radiation Through Atmospheric Turbulence", RADC-TR-74-183, May 1974.

6. V. A. Banakh, et al, J. Opt. Soc. Am. 64, 516-518, April 1974.

7. J. R. Dunphy and J. R. Kerr, J. Opt. Soc. Am. 63, 981-986, August 1973.



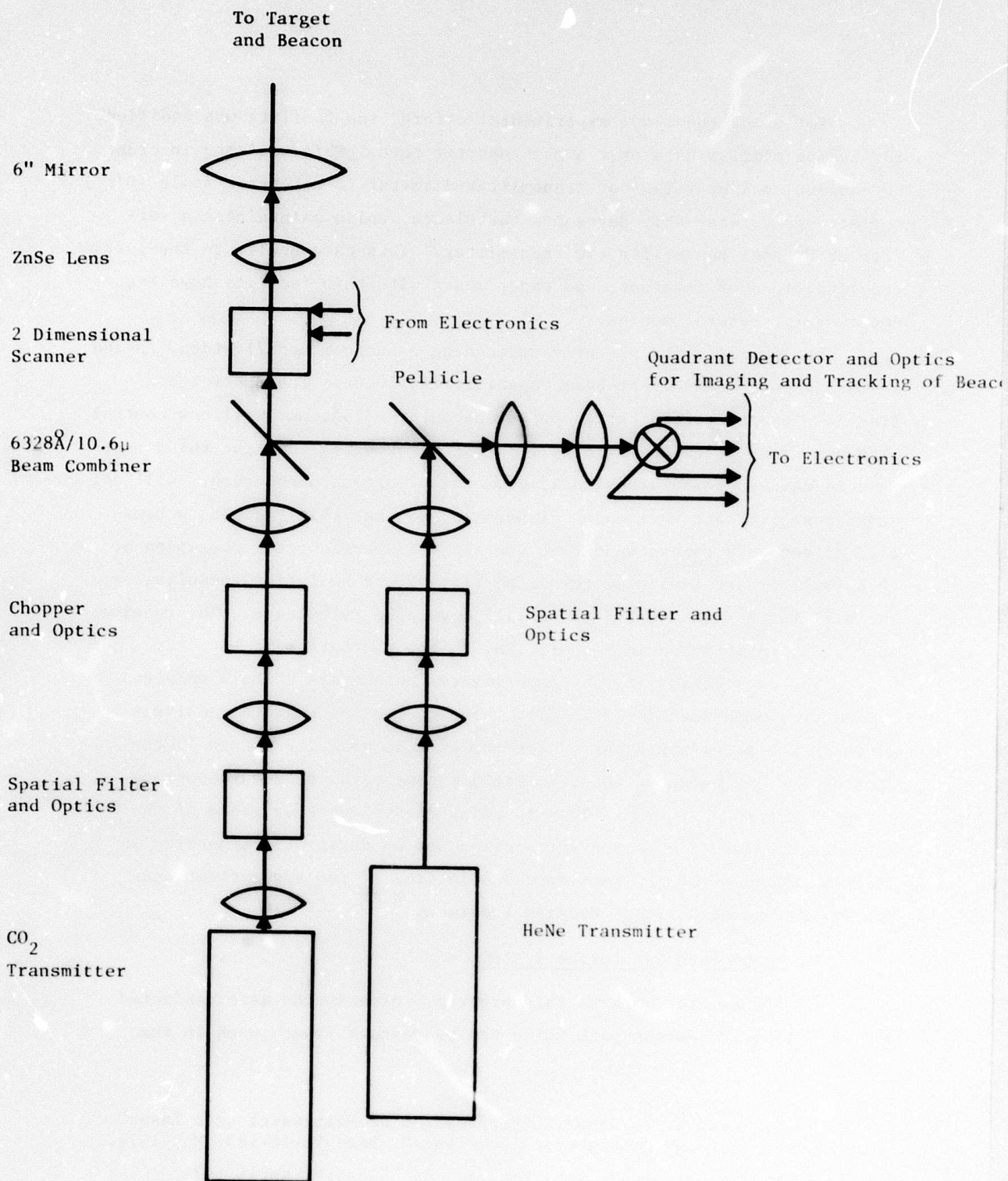


Figure 10. Diagram of multiwavelength tracking transmitter for beam-wander-cancellation and target-irradiance experiments.



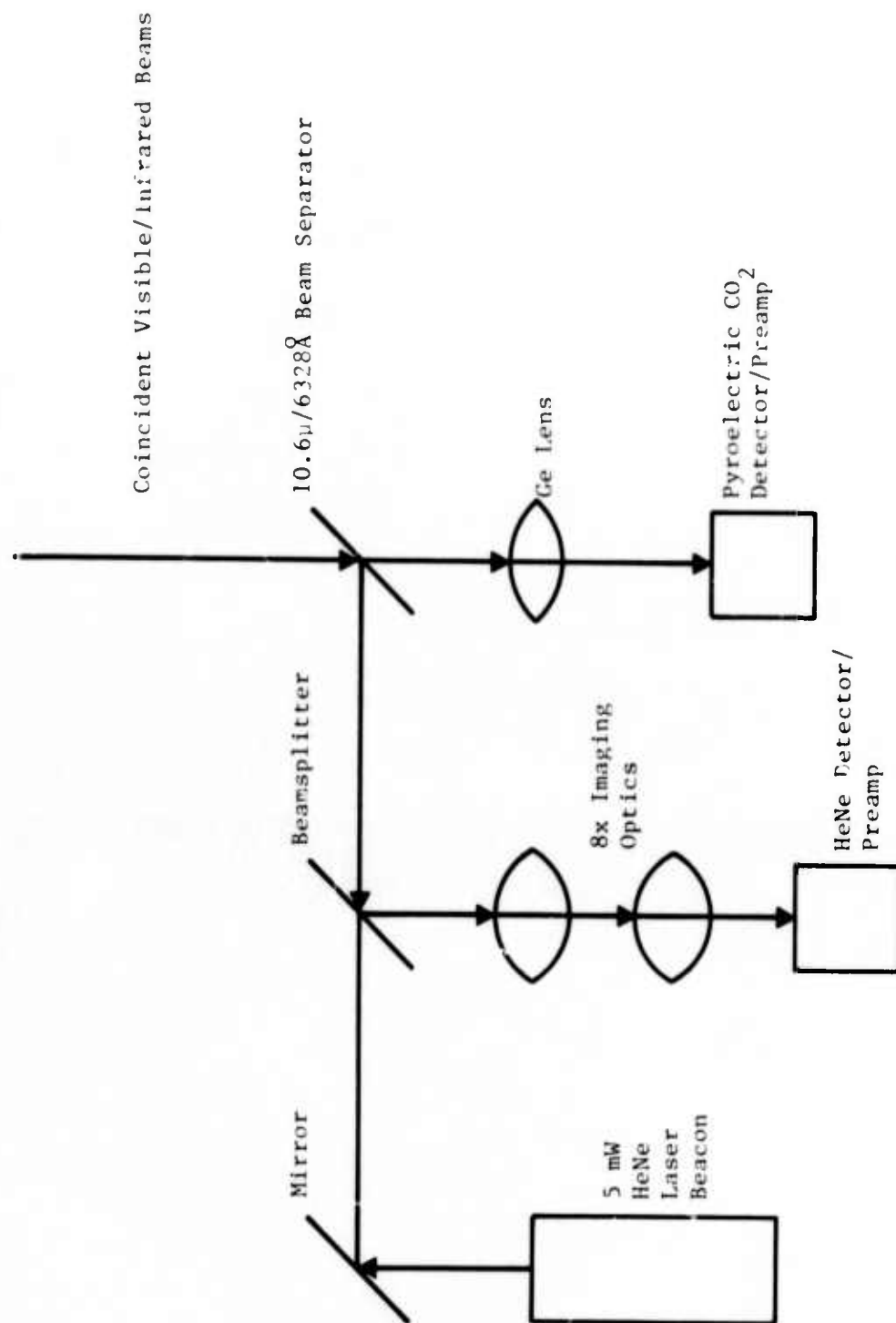


Figure 11. Diagram of multiwavelength receiver for beam-wander-cancellation and target-irradiance experiments.



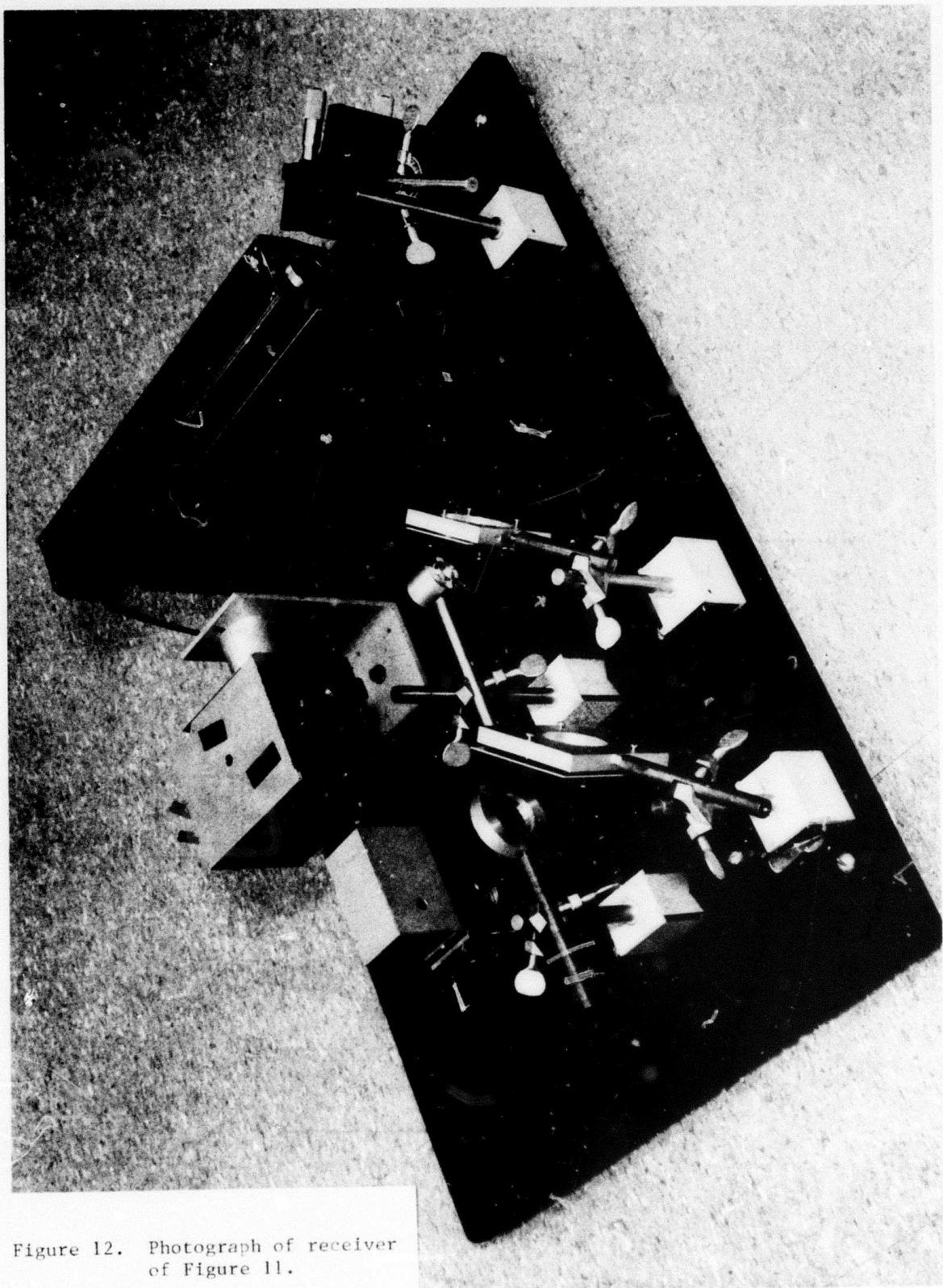


Figure 12. Photograph of receiver  
of Figure 11.



TABLE VII

## Experimental Data and Parameters for Multiwavelength Target-Irradiance System

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Tracker: Wander signals

Target: Linear irradiance fluctuations  
Mean linear irradiance  
Log irradiance fluctuations  
 $C^2$  and microthermal fluctuations  
Meteorological conditions

Processing: Statistics and spectra of fluctuations

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Wavelength:  $6328\text{\AA}$  and  $10.6\mu$  (simultaneous, coincident beams)

Path: 91 m, homogeneous

Beam height: 1.8 m

Mean irradiance: 120 s averaging

Variance { Linear irradiance: 120 s averaging  
Log amplitude  
Wander angle

Spectra: Digital; 0.1 Hz resolution; 100 s averaging

Analog; 1.0 Hz resolution; 100 s averaging

Probability distributions: Digital

Digital sampling rate: 1 kHz

Target receiver: Quasi-Point-Aperture at each wavelength

Target receiver bandwidth: 1 kHz

Target receiver dynamic range: 80 db at  $6328\text{\AA}$ ; 60db at  $10.6\mu$ 

Tracking transmitter aperture: 15.2 cm

Tracking transmitter focus resolution:  $2.5\mu\text{m}$ 

Steering servo resonant frequency: 300 Hz, no load

Steering servo linearity: &lt;1% of peak-to-peak deflection

Steering servo repeatability: 0.050% of peak-to-peak deflection

Open loop transfer function: Single integration

Closed loop bandwidth: 20 Hz

Noise limited tracking angle: <2% of transmitter diffraction-limited width  
( $6328\text{\AA}$ )Transmitter Chopping: 9kHz at  $10.6\mu$  (direct-coupled at  $6328\text{\AA}$ )

Microthermal probe averaging time: 300 s



presence of earth curvature and atmospheric refraction. In this effort, which was undertaken for a better understanding of strong turbulence scattering ("hard saturation" of scintillations), it was determined that multikilohertz fluctuations and correspondingly small amplitude patches exist in the scattered field, in agreement with concurrent theoretical developments.<sup>8</sup> These phenomena are also under intensive study by Russian investigators.<sup>9</sup>

We have re-established the long-path facility, and are currently completing modifications on the original system which will permit a much larger receiver bandwidth and very small apertures ( $\ll \rho_0$ ), in order to fully accommodate the spatial and temporal characteristics of the field. The system operates at 4880Å as before, but with 100 kHz chopping using a novel photoelastic modulator (Fig. 13), and a final (demodulated) bandwidth of 10 kHz. Photomultipliers are utilized to achieve a 100 dB SNR with the small receivers, and the original (dual) covariance receiver has been modified for high resolution at small separations. A new demodulator with the required bandwidth and linear phase response for undistorted transients has been designed with an 80 dB dynamic range.

The system parameters are summarized in Table VIII. The means utilized to achieve high resolution of the covariance are shown in Figure 14. The demodulator, shown in Figure 15, uses a Motorola Type 1496 balanced modulator with a Signetics 565 phase-locked-loop to supply the necessary constant-carrier input; the latter component functions properly over a very large dynamic range, so that severe fading will not interrupt the system. The required phase or transient response is obtained in a four-pole Bessel low-pass filter.

### C. Further Plans

Following the efforts described above, the wander-tracking system will be modified to study the effects of enhanced "angular

8. H. T. Yura, J. Opt. Soc. Am. 64, 59-67, January 1974

9. M. E. Gracheva, et al, "Similarity Correlations and Their Experimental Verification in the Case of Strong Intensity Fluctuations of the Laser Radiation", preprint, August 1973.



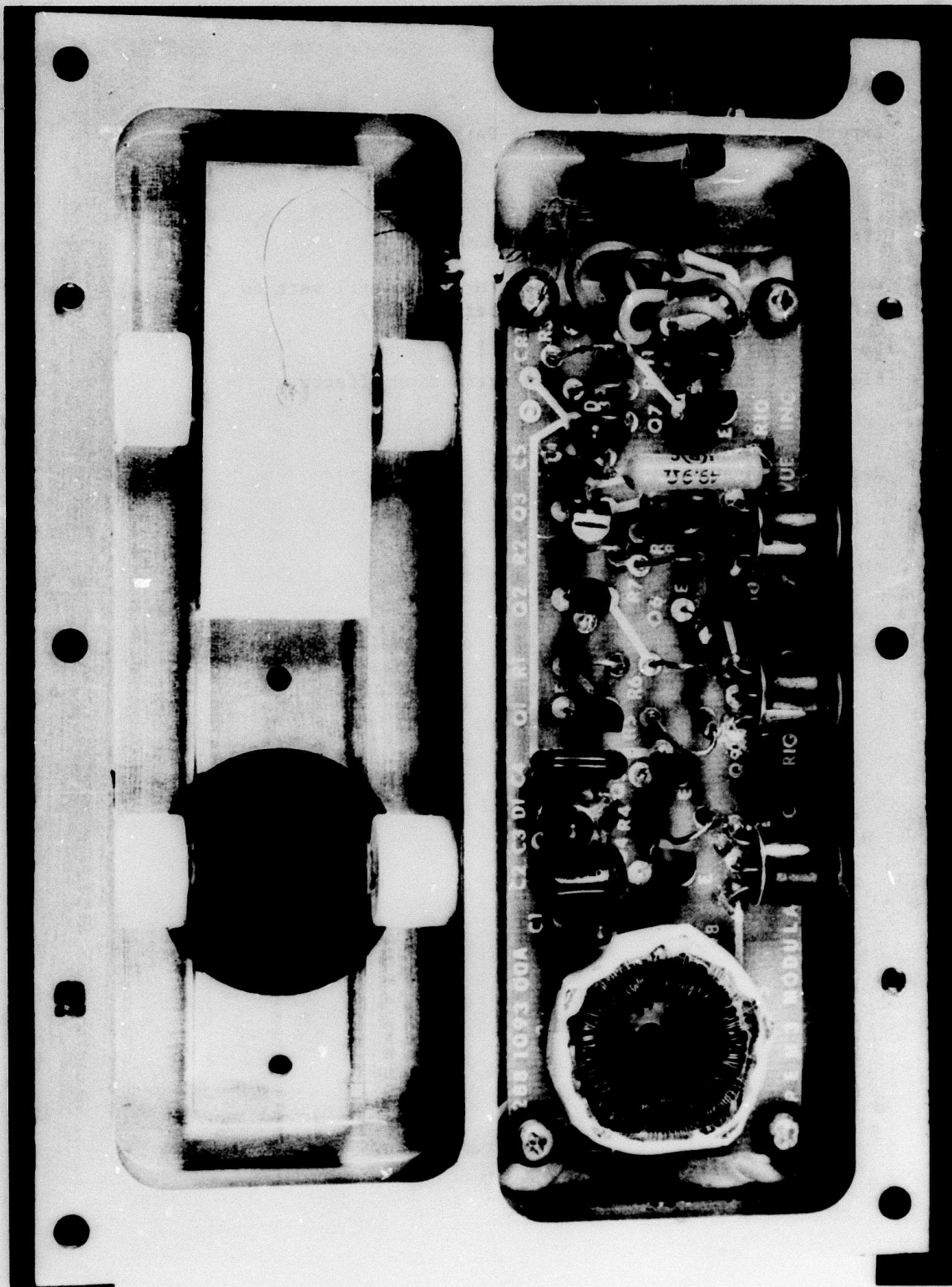


Figure 13. Photoelastic modulator for 100kHz chopping.



TABLE VIII

Experimental Parameters for Long-Path System

Transmitter Characteristics

Wavelength:  $4880\text{\AA}$  Power: 1 watt cw  
Virtual-point-source (Fresnel number = 0.002)  
Chopping rate: 100 kHz  
Height: 7m  
Electronic steering for diurnal refraction effects

Receiver Characteristics

Height: 4m  
Diameter: 0.25mm-1mm  
Minimum covariance separation: 0.25mm  
Bandwidth: 10 kHz  
Dynamic Range: > 80 dB  
Processing:

Variance of log amplitude  
Covariance  
Statistics  
Spectra



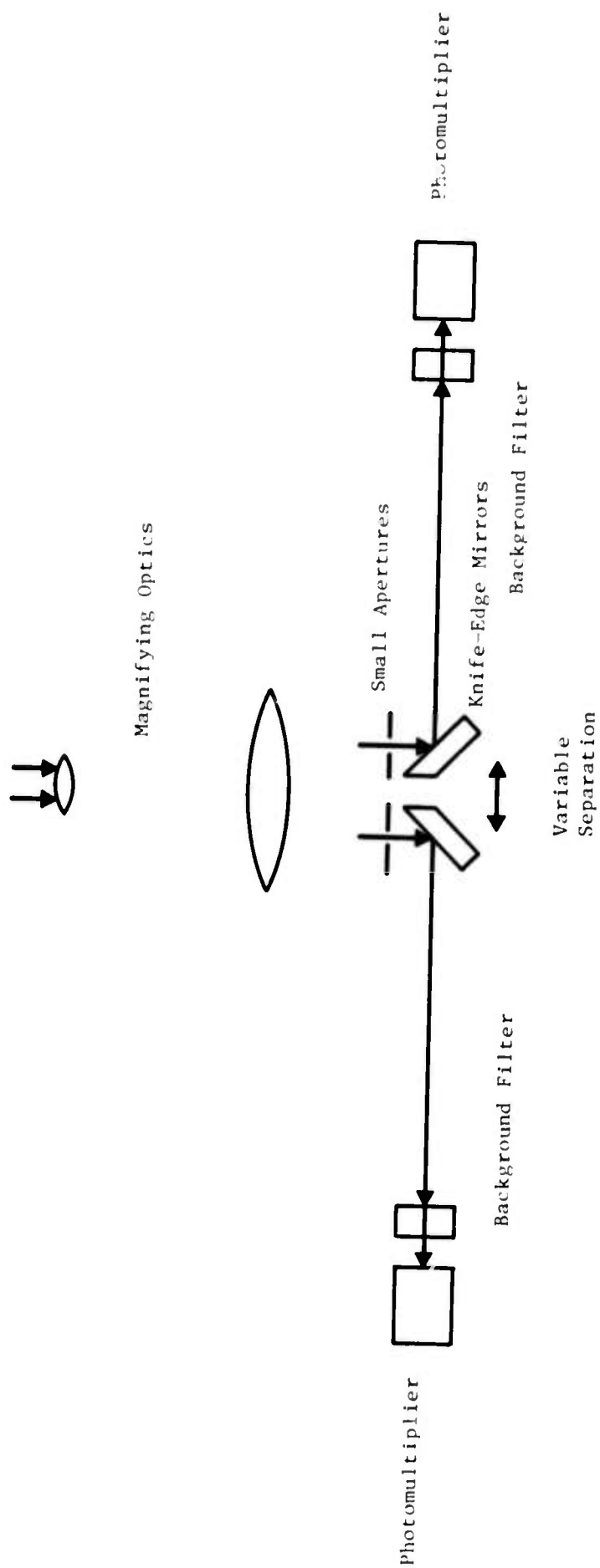


Figure 14. Diagram of high-resolution covariance receiver for long-path, strong-saturation measurements.



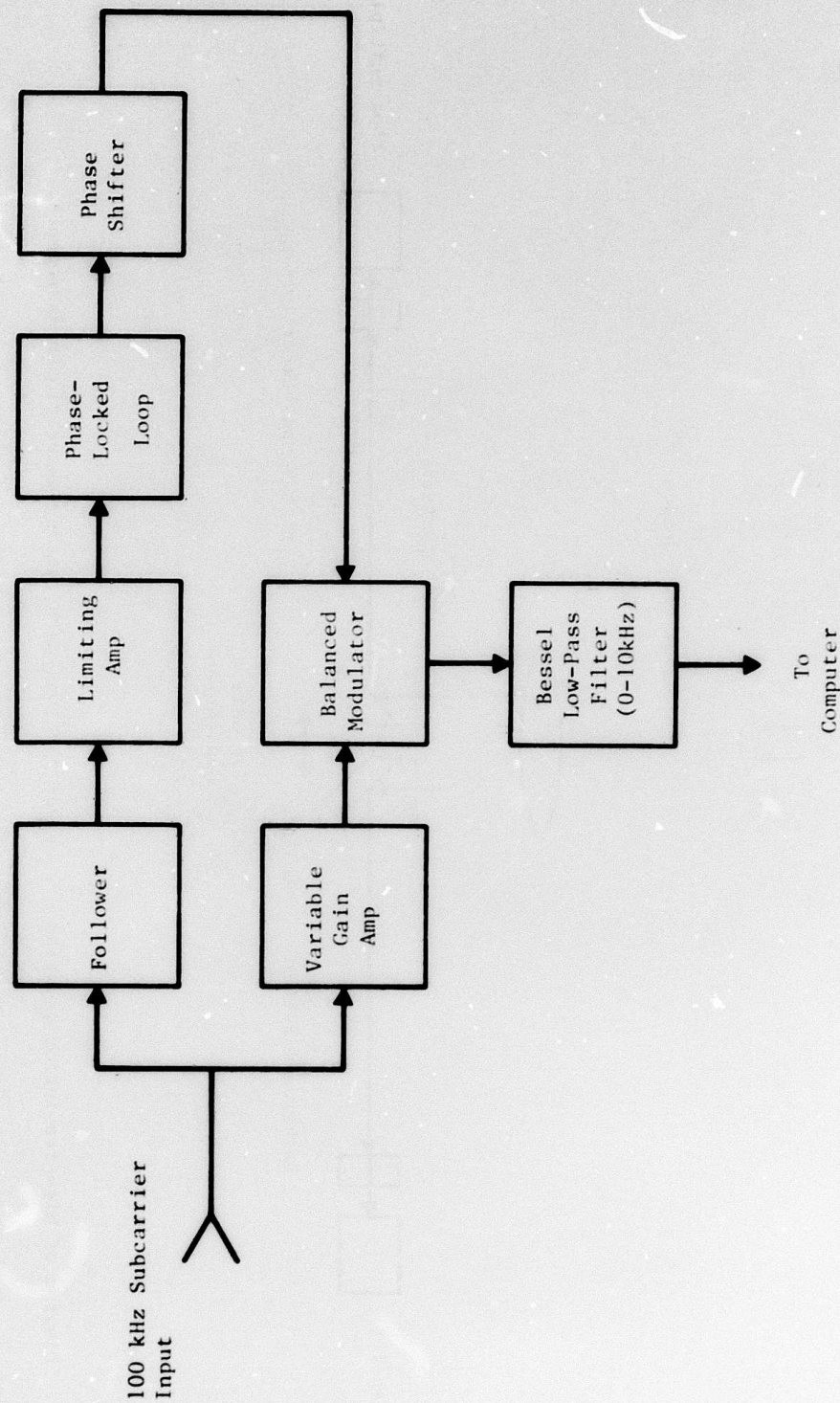


Figure 15. Diagram of wideband, large-dynamic-range demodulator.



scintillation" from a retroreflector.<sup>10,11</sup> Also, in a follow-on effort, the scintillation characteristics including covariance structure will be determined for extended, partially coherent (i.e., generalized) sources. This topic pertains to turbulence effects on "speckle" and has not been adequately understood; it pertains to such applications as remote sensing, and noise in adaptive transmitters.

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10. J. P. Hansen and S. Madhu, Applied Optics 11, 233-238, February 1972.
11. R. F. Lutomirski, Applied Optics 14, 840-846, April 1975.



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3. J. W. Strohbehn, T. Wang, and J. P. Speck, Radio Science 10, 59-70, January 1975.
4. M. Abramowitz and I. Stegun, ed., Handbook of Mathematical Functions, Dover Publications, Inc., N. Y., 931-940, 1965.
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10. J. P. Hansen and S. Madhu, Applied Optics 11, 233-238, February 1972.
11. R. F. Lutomirski, Applied Optics 14, 840-846, April 1975.





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